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1 TITLE:

2 Microfluidic Model to Mimic Initial Event of Neovascularization

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KEYWORDS:

33 neovascularization, microfluidics, shear stress, microenvironment, transendothelial flow, 3D

34 culture

35 36

SUMMARY:

Here, we provide a microfluidic chip and an automatically controlled, highly efficient circulation microfluidic system that recapitulates the initial microenvironment of neovascularization,

- allowing endothelial cells (ECs) to be stimulated by high luminal shear stress, physiological level
- 40 of transendothelial flow, and various vascular endothelial growth factor (VEGF) distribution
- 41 simultaneously.

42 43

ABSTRACT:

44 Neovascularization is usually initialized from an existing normal vasculature and the

biomechanical microenvironment of endothelial cells (ECs) in the initial stage varies dramatically from the following process of neovascularization. Although there are plenty of models to simulate different stages of neovascularization, an *in vitro* 3D model that capitulates the initial process of neovascularization under the corresponding stimulations of normal vasculature microenvironments is still lacking. Here, we reconstructed an *in vitro* 3D model that mimics the initial event of neovascularization (MIEN). The MIEN model contains a microfluidic sprouting chip and an automatic control, highly efficient circulation system. A functional, perfusable microchannel coated with endothelium was formed and the process of sprouting was simulated in the microfluidic sprouting chip. The initially physiological microenvironment of neovascularization was recapitulated with the microfluidic control system, by which ECs would expose to high luminal shear stress, physiological transendothelial flow, and various vascular endothelial growth factor (VEGF) distributions simultaneously. The MIEN model can be readily applied to the study of neovascularization mechanism and holds a potential promise as a low-cost platform for drug screening and toxicology applications.

INTRODUCTION:

 Neovascularization happens in many normal and pathological processes ^{1–4}, which include two major processes in adults, angiogenesis and arteriogenesis ⁵. Besides the best-known growth factors, such as vascular endothelial growth factor (VEGF) 6, mechanical stimulations, in particular the blood flow induced shear stress is important in the regulation of neovascularization 7. As we know, the magnitude and forms of shear stress vary dramatically and dynamically in different parts of the vasculature, resulting in important effects on vascular cells ^{8–12}. Previous studies have shown that shear stress may affect various aspects of ECs, including cell phenotypic changes, signal transduction, gene expression, and the communication with mural cells ^{13–20}; hence, regulate neovascularization ^{21–24}.

Therefore, to better understand neovascularization, it is important to reconstruct the process in natural cellular microenvironment in vitro. Recently, many models have been established to create micro-vessels and provide precise control of microenvironment^{25–27}, taking advantage of advances in microfabrication and microfluidic technology. In these models, micro-vessels can be generated by hydrogel^{28,29}, polydimethylsiloxane (PDMS) microfluidic chips^{30–32} or 3D bioprinting^{33,34}. Some aspects of the microenvironment, such as luminal shear stress^{22,23,35,36}, transendothelial flow^{37–40}, biochemical gradient of angiogenic factors^{41,42}, strain/stretch^{43–45}, and co-cultured with other types of cells^{32,46} have been mimicked and controlled. Usually, a large reservoir or syringe pump was used to provide perfused medium. Transendothelial flow in these models was created by pressure drop between the reservoir and micro-tube^{22,23,38,40}. However, the mechanical microenvironment is hard to maintain constantly in this way. Transendothelial flow would increase and then exceed the physiological level if a high flow rate with high shear stress was used for perfusion. Previous study showed that at the initial period of neovascularization, the velocity of transendothelial flow is very low due to the intact ECs and basement membrane, usually under 0.05 µm/s8. Meanwhile, though luminal shear stress in vascular system varies greatly, it is relatively high with mean values of 5-20 dyn/cm^{2-11,47}. For now, the velocity of transendothelial flow in previous works have been generally kept between 0.5-15 μm/s^{22,38-40}, and the luminal shear stress was usually under 10 dyn/cm^{2 23}. It remains a

difficult subject to constantly expose ECs to high luminal shear stress and physiological level of transendothelial flow simultaneously.

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In the present study, we describe an *in vitro* 3D model to mimic the initial event of neovascularization (MIEN). We developed a microfluidic chip and an automatic control, highly efficient circulation system to form perfusion micro-tubes and simulate the process of sprouting⁴⁸. With the MIEN model, the microenvironment of ECs stimulated at the initial period of neovascularization are firstly recapitulated. ECs can be stimulated by high luminal shear stress, physiological level of transendothelial flow and various VEGF distribution simultaneously. We describe the steps of establishing the MIEN model in detail and the key points to be paid attention to, hoping to provide a reference for other researchers.

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PROTOCOL:

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1. Wafer preparation

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NOTE: This protocol is specific for the SU-8 2075 negative photoresist used during this research.

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1.1. Clean the silicon wafer 3 to 5 times with methanol and isopropanol on a spin coater as follows: first spin for 15 s at 500 rpm, then spin for 60 s at 3,000 rpm.

109

1.2. Transfer the silicon wafer to a hotplate, which preheated to 180 °C and bake the wafer for 10 min.

112

1.3. Remove the silicon wafer from the hotplate and cool it to room temperature. Clean the wafer again with compressed air before proceeding with the spin coating. Apply 4 mL of the SU-8 2075 photoresist to the center of the wafer.

116

1.4. Obtain a feature height of 70 μ m on the spin coater as follows: first spin for 12 s at 500 rpm, then spin for 50 s at 2,100 rpm.

119

1.5. Soft bake the wafer on a hotplate as follows: first bake for 8 min at 65 °C, then bake for 20 min at 95 °C. Next, remove the silicon wafer from the hotplate and cool it to room temperature before lithography.

123

1.6. Place a photomask onto the photoresist film. Expose the wafer with a lithography equipment to achieve a total exposure of 200 mJ/cm².

126

NOTE: The photomask contains nine sets of patterns of the chip, so it can fabricate nine microfluidic sprouting chips each time.

- 130 1.7. Post exposure the wafer on a hotplate as follows: first bake for 5 min at 65 °C, then bake
- 131 for 20 min at 95 °C. Next, remove the silicon wafer from the hotplate and cool it to room
- 132 temperature before developing.

134 1.8. Transfer the wafer to a glass Petri dish filled with SU-8 developer (PGMEA) to start developing.

136

137 CAUTION: The developer is irritating to the eyes and respiratory tract. Perform developing in a fume hood. Wear splash goggles, nitrile gloves, and airline mask during the operation.

139

140 1.9. Shake the dish gently along the direction of the flow channel and change the developer after 10 min.

142

1.43 1.10. Repeat step 1.9 for 3–5 times until the patterns can be clearly observed.

144

NOTE: Make sure there is no photoresist residue left on the wafer, otherwise rinse the wafer in the developer again.

147

148 1.11. Transfer the wafer to a preheated hotplate set to 120 °C and bake it for 30 min.

149

1.12. Pipet 35 μL of silane onto a coverslip, then put the coverslip along with the wafer into a
 desiccator and pull vacuum. Seal the desiccator and leave the wafer under vacuum for 4 h to
 silanize the wafer to prevent the adhesion of PDMS during the soft-lithography processes.

153

154 CAUTION: The silane is toxic. To prevent poisoning, perform silanization in the fume hood and wear nitrile gloves while handling.

156

157 1.13. Release the vacuum from the desiccator. Remove the silanized wafer onto a preheated hotplate and bake it at 65 °C for 2 h.

159

160 1.14. Store the wafer in a clean Petri dish until required.

161

2. Microfluidic sprouting chip fabrication

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2.1. Combine 20 g of base agent and 2 g of curing agent (10:1 ratio) in a plastic beaker and mix them thoroughly with a mixing rod.

166

2.2. Place the beaker into a desiccator and pull vacuum for 1 h to remove air bubbles in the PDMS mixture.

169

2.3. Pour the PDMS mixture onto the wafer in the Petri dish and place the Petri dish back into the desiccator, degassing for another 30 min.

172

NOTE: It is helpful to use double-sided adhesive tape to glue the wafer onto the bottom of the Petri dish to ensure the wafer is kept horizontal during degassing and curing.

175

176 2.4. Remove the Petri dish from the desiccator and place it into an 80 °C dry oven for 3 h to

177	cure.					
178						
179	2.5.	Carefully separate the PDMS layer from the wafer and cut the layer to nine chips with a				
180	scalpel according to the pattern.					
181						
182	NOTE: Keep the feature side up after separation.					
183						
184	2.6.	Punch two hydrogel injection ports and four media injection ports out of each chip using				
185	a 1 mm	n and a 3.5 mm biopsy punch, respectively.				
186						
187	2.7.	Clean the punched chips with residue-free tape to remove PDMS residue. Place the chips				
188	and nii	ne glass coverslips into a plasma cleaner and treat them with oxygen plasma for 30 s to				
189	form covalent bonding on the surface.					
190						
191	2.8.	Take out the chips and coverslips. Attach the feature side of the chips onto the coverslips.				
192						
193	2.9.	Place the attached chips into an 80 °C dry oven for 1 h to intensify the bonding.				
194						
195	2.10.	Autoclave the chips before use and keep them sterile for the rest of the procedure.				
196						
197	3. Sur	face modification and hydrogel injection				
198						
199	3.1.	For each chip, pipet 40 μL of 1 mg/mL poly-D-lysine (PDL) and inject it into channels in the				
200	chip from hydrogel injection port.					
201	•					
202	NOTE:	Make sure the PDL fills channels, especially in narrow channels near the ports.				
203						
204	3.2.	Incubate the chips at 37 °C for 4 h to modify the surface of the PDMS.				
205						
206	3.3.	Pipet 200 μL of sterile water and inject it into channels in the chip from hydrogel injection				
207	port to	wash out PDL.				
208	•					
209	3.4.	Remove the chips into a 120 °C dry oven for 3 h to restore hydrophobicity.				
210		, , , , , , , , , , , , , , , , , , , ,				
211	3.5.	Place on ice a sterile tube and calculate the volume of Type I collagen to be used as the				
212	followi	ng equation.				
213		Final volume (50 μL) x Final collagen concentration (3 mg/mL in this research) /				
214		Concentration in bottle = volume collagen to be added				
215						
216	3.6.	Calculate the volume of NaOH to be used as the following equation.				
217	-	(volume collagen to be added) x 0.023 = volume 1 N NaOH				
218		(1.2 1.2 1.2. 1.2.1.2.2.)				
219	3.7.	Prepare 50 μL of hydrogel in the tube as the following protocol: add 5 μL of 10x PBS, 0.5				
220		henol red, calculated volume of 1 N NaOH, 4 μL of 1 mg/mL Fibronectin, calculated volume				

- of Type I collagen in turn. Add proper amount of dH_2O so that the total volume reaches 50 μ L.
- 222 Mix all the contents in the tube thoroughly.

- NOTE: Perform all the operations on ice. Use phenol red as an acid-based indicator to assist in
- visual determination of the pH of the hydrogel. The final hydrogel ends up orange when the pH
- is about 7.4 and the stiffness is about 15 kPa⁴⁹.

227

228 3.8. Pipet 2–3 μ L of hydrogel for each chip and slowly inject it into the central hydrogel 229 channel from hydrogel injection port.

230

3.9. Incubate the chips at 37 °C for 30 min to allow gelation.

232

- NOTE: Seal the chips into a sealed box with 1 mL of sterile water if they are not used immediately.
- 234 Sealed chips can be stored at 37 °C for at most 24 h.

235

236 4. Cell seeding

237

238 4.1. Pipet 20 μ L of 125 μ g/mL Fibronectin into one media injection port of the cell culture 239 channel.

240

241 4.2. Cut a pipette tip to fit the port of the cell culture channel with scissors.

242

4.3. Insert the pipette tip into the other media injection port of the cell culture channel. Then,pipet out air from the cell culture channel to fill it with Fibronectin.

245

246 4.4. Incubate the chips at 37 °C for 1 h.

247

248 4.5. Before cell seeding, pipet 20 μ L of ECM media into each media injection port and incubate 249 the chips at 37 °C for 30 min.

250

4.6. Then, pipet out all the media in all media injection ports.

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- 253 4.7. Next, pipet 5 μ L of cell suspension into one media injection port of cell culture channel.
- 254 Then, endothelial cells quickly spread over the entire channel under differential hydrostatic

pressure.

256

- NOTE: Prepare the cell suspension by trypsinizing human umbilical vein endothelial cells
- 258 (HUVECs) from the culture flask and centrifuging them at 400 x g. Then, resuspend the cells to
- 259 10⁷ cells/mL in a tube.

260

261 4.8. Add about 4–6 μ L of ECM media to the other port to adjust the hydrostatic pressure and 262 stop cell moving.

263

264 4.9. Remove the chips to the cell incubator. Then, turn over the chips every 30 min until

- 265 endothelial cells coat around the internal surface of the cell culture channel 2 h later (**Figure 1**).
- NOTE: To make the chip upside down, pipet a little water on the back of the coverslip then the chip can attach to the cover of the Petri dish.
- 4.10. Use the pipette tip to remove the attached cells in the injection ports very carefully.
- 4.11. Then, insert four barbed female Luer adaptors into the media injection ports and fill with ECM media.
- NOTE: The adaptors can function as fluid reservoirs to provide nutrients for the cells in the channel.
- 278 4.12. Remove the chips to cell incubator. Change ECM media in Luer adaptors every 12 h.

280 **5.** Measurement of FITC-dextran diffusional permeability

- NOTE: To assess barrier function of the micro-vessel, diffusional permeability of the EC culture channel with or without cell lining is assessed.
- 285 5.1. Take out a microfluidic sprouting chip with hydrogel injected. 286
- 287 5.2. Repeat steps 4.1–4.6.

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- 289 5.3. Remove all the Luer adaptors and pipet out all the media in four media injection ports. 290
- 291 5.4. Place the chip onto the confocal laser scanning microscope.
- 293 5.5. Pipet 5 μ L of culture media containing 500 μ g/mL 40 kDa FITC-dextran to one port of cell culture channel.
- NOTE: 40 kDa FITC-dextran has similar molecular size to VEGF-165 (39–45 kDa).
- 298 5.6. Capture images every 3 s for 30 s. Thus, the diffusional permeability without cell lining is measured.
- 301 5.7. Take out microfluidic sprouting chip after HUVECs are confluent in the cell culture 302 channel.
- 304 5.8. Repeat steps 5.3–5.5.
- 306 5.9. Capture images every 3 s for 30 s. Thus, the diffusional permeability with cell lining is 307 measured. 308

5.10. Calculate the diffusional permeability by quantifying changes of fluorescent intensity over time using the following modified equation⁵⁰.

311
$$P_d = (I_2 - I_1) / ((I_1 - I_b) \cdot \triangle t) \cdot S/d$$

where, P_d is diffusional permeability coefficient, I_1 is average intensity at an initial time point, I_2 is average intensity after delta time ($\triangle t$), I_b is background intensity, S is the area of the channel in fluorescence images, and d is the total interval of micro-posts in fluorescence images. In the present work, $\triangle t$ is set as 9 s.

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318

NOTE: The present equation is slightly different from the original⁵⁰, due to the diffusion direction of the fluorescence in the chip is only from the EC channel to hydrogel channel, which is not like the circular tube diffusing in all the radial direction.

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6. Microfluidic control system setup

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NOTE: The microfluidic control system in the present study is consisted of a micro-syringe pump, an electromagnetic pinch valve, a bubble trap chip, a microfluidic chip, a micro-peristaltic pump, and a reservoir. Each part of the system can be replaced by alternatives able to perform the same function.

326327

328 6.1. Bubble trap chip fabrication

329

NOTE: The bubble trap chip is used to remove air bubbles in circulation. The chip consists of three PDMS layers. The top layer is constructed using soft lithography to form grid structure as the liquid chamber. Each channel of the grid structure is $100 \mu m$ wide. The bottom layer is a PDMS chunk with a hole. Between the two layers, a $100 \mu m$ thin PDMS film is laid.

334

335 6.1.1. Repeat step 1 to prepare the wafer for bubble trap chip.

336

337 6.1.2. Repeat steps 2.1–2.5 to fabricate the top layer and bottom layer of the bubble trap chip.

338

NOTE: The photomask of the top layer contains three sets of patterns, so cut the PDMS layer to three chips according to the pattern.

341

6.1.3. Punch six holes on the end of inlet and outlet channels of the top layer using a 3.5 mm biopsy punch.

344

6.1.4. Punch two holes on the corresponding position of bottom layer using a 6 mm biopsy punch according to the pattern on the top layer.

347

348 6.1.5. Repeat steps 2.1–2.2 to prepare 10 g of PDMS mixture and pour it on the center of a cleaned silicon wafer.

350

6.1.6. Fabricate a 100 μ m PDMS film by applying the following spin protocol: spin for 15 s at 500 rpm, increase the spin speed to 1,300 rpm and hold here for 45 s.

354 6.1.7. Transfer the wafer to a preheated hotplate set to 180 °C and bake it for 30 min.

355

356 6.1.8. Clean the punched layers with residue-free tape to remove PDMS residue. Place the top
357 layers and wafer into a plasma cleaner and treat them with oxygen plasma for 30 s to form
358 covalent bonding on the surface.

359

360 6.1.9. Take out top layers and wafer. Attach the feature side of top layers onto the PDMS film.

361

362 6.1.10. Cut the film carefully along the edge of the top layers with a needle.

363

364 6.1.11. Slowly separate the film from the wafer and turn over the chips to make the film side up after separation.

366

6.1.12. Place the bottom layers and attached chips into a plasma cleaner and treat them with oxygen plasma for 30 s again.

369

6.1.13. Take out bottom layers and attached chips. Attach the bottom layers onto the PDMS filmand the bubble trap chips are done.

372

NOTE: Align the holes on the bottom layer with the patterns on the top layer when attaching.

374

376

- 375 6.1.14. Place the chips into an 80 °C dry oven for 1 h to intensify the bonding.
- 377 6.2. Assemble the microfluidic control system

378

NOTE: All the parts of the system, such as bubble trap chip, reservoir, tubes, and connectors are used after autoclave sterilization, except electronic equipment. Assemble the microfluidic control system on a clean bench.

382

6.2.1. To assemble the microfluidic control system, prepare two polytetrafluoroethylene tubes, two short silicone tubes, three long silicone tubes, one barbed female Luer adaptor, one Y type connector, and three L type connectors.

386

NOTE: The advantage of polytetrafluoroethylene tube is low elasticity, therefore, less media is needed in pipeline. Silicone tube, in contrast, has high elasticity, therefore, it is suitable for the pinch valve and peristaltic pump.

390

391 6.2.2. Fill the syringe with 10 mL of preheated (37 °C) ECM medium.

392

NOTE: Preheating helps the medium release dissolved gas.

- 395 6.2.3. Connect a polytetrafluoroethylene tube to the syringe by a barbed female Luer adaptor.
- 396 Then, connect the other end of polytetrafluoroethylene tube to a Y type connector.

398 6.2.4. Next, connect two long silicone tubes to the other two ends of Y type connector with one tube connecting to the reservoir and the other tube connecting to the bubble trap chip.

400

401 6.2.5. Connect another long silicone tube to the reservoir.

402

403 6.2.6. Next, use two short silicone tubes to connect all inlet and outlet holes on the top layer of the bubble trap chip. Connect a polytetrafluoroethylene tube to the backend of the chip.

405

406 6.2.7. Next, fix the syringe onto the micro-syringe pump.

407

408 6.2.8. Clip two long silicone tubes into the electromagnetic pinch valve.

409

410 6.2.9. Next, switch the electromagnetic pinch valve to open the pipeline between the syringe 411 and the reservoir. Inject the media to the reservoir using a micro-syringe pump to exhaust air in 412 the tube.

413

6.2.10. Then, switch the valve again to open the pipeline between the syringe and the bubble trap chip. Inject the media to fill the liquid chamber and the backend tube of the bubble trap chip.

417

7. Endothelial sprouting assay

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NOTE: A stage top incubator assembled with phase contrast microscope is used in the present study to observe the process of sprouting in real time. The stage top incubator can maintain the temperature, humidity, and CO₂ control on microscope stages, being good for live cell imaging. But the equipment is not necessary for the assay. The protocols provided here can also be worked in a basic cell incubator.

425

426 7.1. Take out endothelial sprouting chips from the cell incubator.

427

7.2. Then, remove Luer adaptors on the cell culture side. Insert two pipe plugs into the hydrogel injection ports of the microfluidic sprouting chip.

430

NOTE: The plugs can transform from needles and their main function is to prevent media from spilling.

433

434 7.3. Connect the backend tube of bubble trap chip to one port of cell culture channel.

435

436 NOTE: Make sure there are no bubbles in the tube before connection.

437

438 7.4. Insert a T type connector to the other port and connect it to long silicone tube connected 439 with the reservoir.

441 7.5. Clip the long silicone tube into the micro-peristaltic pump.

442

443 7.6. Then, insert an air filter to the reservoir.

444

445 7.7. Next, assemble the microfluidic sprouting chip to the stage top incubator.

446

447 7.8. Next, connect the vacuum pump to the holes in the bottom layer of bubble trap chip by 448 a TPU tube.

449

450 7.9. Set up the circulation volume and flow rate in the custom program which controls the 451 micro-syringe pump and electromagnetic pinch valve simultaneously (Figure 2).

452

453 NOTE: The flow rate across the endothelial cell culture channel is calculated according to the 454 classic equation.

455

 $\tau = 6\mu Q / Wh^2$ where, τ is shear stress (dyn/cm²), μ is viscosity of the medium (8.8 x 10⁻⁴ Pa · s), Q is the flow rate

456 457 458 459

- across the endothelial cell culture channel (ml/s), h is channel height (70 µm), and W is channel width (1,000 μm). The viscosity of the medium is measured using a coaxial cylinder type rotational viscometer. The height and width of the channel are predetermined and manually confirm using a phase contrast microscope at 4x magnification. The circulation volume is 5 mL
- 461 and flow rate is 85 µL/min (average 0.2 m/s in cell culture channel) for 15 dyn/cm² shear stress
- 462 according to calculation.

463

460

464 7.10. Next, set up the flow rate of micro-peristaltic pump.

465

466 NOTE: The flow rate of micro-peristaltic pump is slightly higher than micro-syringe pump, in order 467 to prevent the media from spilling.

468

469 7.11. Turn on the micro-syringe pump. Then, the circulation control system is established.

470

8. Data analysis

471 472

473 NOTE: To quantify the sprouts, the normalized area of sprouting, average sprout length, and 474 longest sprout length were calculated. Results represent mean ± SEM obtained from three 475 independent studies. Statistical significance (P < 0.05) is assessed by Student's t-test.

476

- 477 Fix cells and sprouts in the microfluidic sprouting chip after experiments with 4% 8.1. 478 paraformaldehyde in PBS for 15 min. Stain nuclei with 4',6-diamidino-2-phenylindole 479 dihydrochloride (DAPI; 1: 1000; Sigma-Aldrich) for 10 min and then stain cytoskeleton with TRITC
- 480 phalloidin (P5285, 1: 100; Sigma-Aldrich) for 1 h. Wash cells with PBS three times at 5 min
- 481 intervals between each step.

482

483 8.2. Take confocal images of the chips in a tiling mode and stitch them using image editing 484 software.

8.4. Manually identify and label each tip of sprouts in Z-projection images and calculate distances between sprouts tips to ECs basement membrane using another custom code to quantify average sprout length and longest sprout length (See **Supplemental File**).

REPRESENTATIVE RESULTS:

The in vitro 3D model to mimic the initial event of neovascularization (MIEN) presented here consisted of a microfluidic sprouting chip and a microfluidic control system. The microfluidic sprouting chip was optimized from previous publications^{22,23,37,40,51–53}. Briefly, it contained three channels and six ports: an endothelial cell culture channel and a liquid channel with four media injection ports, and a central hydrogel channel with two hydrogel injection ports (Figure 3). The microfluidic control system consisted of a micro-syringe pump, an electromagnetic pinch valve, a bubble trap chip, a micro-peristaltic pump, and a culture medium reservoir (Figure 4). A custom program was used to control the micro-syringe pump and electromagnetic pinch valve simultaneously, with which the flow rate and circulation volume can be set up. A compensation volume was introduced to correct the slight change of volume after multiple cycles due to systemic error. To minimize the medium used for perfusion, an electromagnetic pinch valve was introduced for medium recycle. The electromagnetic pinch valve could switch between two states to make the microfluidic system in two phases in a cycle. In the injection phase, culture medium was slowly injected from the micro-syringe pump to the microfluidic sprouting chip. While in the recycle phase, culture medium was very rapidly extracted from the reservoir back to the micro-syringe pump.

The barrier function of the micro-vessel in our MIEN model was assessed by measuring the diffusional permeability coefficient (P_d) of 40 kDa FITC-dextran. As it is shown in **Figure 5**, the P_d of static cultured chip with cell lining is $0.1 \pm 0.3 \, \mu \text{m/s}$, and the P_d of empty channel without cell lining is $5.4 \pm 0.7 \, \mu \text{m/s}$. Then, endothelial sprouting assay under static and perfusion was performed in the MIEN model. In static conditions, endothelial sprouting occurred about 4 h after seeding and the sprouts would migrate across the central hydrogel channel to the other side in about 48 h. The sprouts degraded gradually after 48 h. While after 24 h of exposure to 5 or 15 dyn/cm² shear stress (average 0.07 or 0.2 m/s in cell culture channel), ECs aligned in the flow direction changing from polygonal, cobblestone shape into fusiform, and the degree of sprouting decreased with the increase of shear stress (**Figure 6**). However, the sprouts under shear conditions were more stable than under static culture conditions. They could maintain over 48 h under perfusion. Quantitative statistics showed that endothelial sprouting decreased significantly in terms of area of sprouting, average sprout length, and longest sprout length (**Figure 7**).

FIGURE AND TABLE LEGENDS:

are evenly dispersed in the cell culture channel 2 h after cell seeding.

Figure 2: The custom program used to control the micro-syringe pump and electromagnetic pinch valve simultaneously. Main page (up) and subpage (down) of the custom program with which the flow rate and circulation volume can be set up. A compensation volume was introduced to correct the slight change of volume after multiple cycles due to systemic error.

Figure 3: The schematic of the microfluidic sprouting chip. The chip contains three channels and six ports: an endothelial cell culture channel and a liquid channel with four media injection ports, and a central hydrogel channel with two hydrogel injection ports.

Figure 4: The schematic of the microfluidic control system. The microfluidic control system consists of a micro-syringe pump, an electromagnetic pinch valve, a bubble trap chip, a microperistaltic pump, and a culture medium reservoir.

Figure 5: Diffusional permeability (P_d **) of 40 kDa FITC-dextran.** The P_d of static cultured chip with cell lining is 0.1 ± 0.3 µm/s, and the P_d of empty channel without cell lining is 5.4 ± 0.7 µm/s. **, p < 0.01.

Figure 6: Representative images of endothelial sprouting under different shear conditions. After 24 h of static culturing, HUVECs invade from the cell culture channel into the adjacent hydrogel channel through micro-posts and a large number of sprouts in the hydrogel. While after 24 h of exposure to 5 or 15 dyn/cm² shear stress, the degree of sprouting decrease obviously.

Figure 7: Quantified area of sprouting, average sprout length, and longest sprout length. After 24 h of static culture (S0) or exposure to 5 (S5) or 15 (S15) dyn/cm² shear stress, the degree of sprouting decrease with the increase of shear stress. *, p < 0.05; **, p < 0.01.

DISCUSSION:

For a long time, real-time observation of neovascularization has been a problem. Several approaches have been developed recently to create perfused vessels lining with ECs and adjacent to extracellular matrix for sprouting^{22,32,40,46,54}, but the mechanical microenvironment is still hard to maintain constantly. It remains a difficult subject to mimic the initial biomechanical microenvironment of ECs, which are subjected to high luminal shear stress and low velocity of transendothelial flow. Here, we presented a MIEN model that firstly simulates the initial event of neovascularization in mimic physiological microenvironment. With the MIEN model, automatic, efficient and bubble-free long-term perfusion is achieved. Luminal shear stress on ECs could be optionally changed at any time during experiments with transendothelial flow staying at physiological level.

The key of the MIEN model is decoupling the effect of luminal flow on ECs from transendothelial flow. To this end, a T-type connector is creatively inserted to the outlet port of the EC culture channel. One end of the connector is connected to the reservoir through the micro-peristaltic pump. The other end of the connector is exposed to the air of the incubator. It keeps pressure

inside the endothelial cell culture channel the same as the atmospheric pressure, since there is neither surplus media gathering to increase pressure nor excess media being drawn away to form negative pressure in the channel. In this way, the flow resistance after microfluidic sprouting chip is very small so that the transendothelial flow can be maintained at physiological range even under high luminal shear stress.

One critical step within the protocol is the successful injection of hydrogel in central hydrogel channel. Huang et al. proposed that successful filling of the gels depends on balancing the capillary forces and surface tension within the microfluidic gel channel⁵⁵. They found three different variables to control the balance: the spacing between micro-posts, the surface properties of the device, and the viscosity of the hydrogel precursor solutions. In the present model, the design of the microfluidic sprouting chip is optimized from previous works^{22,23,37,40,51–53}. The geometry and spacing of micro-posts to separate three channels are determined based on previous calculations and numerous experiments. Further, PDL coating and high temperature baking are performed to modify the PDMS surface; hence, adjust the balance between hydrophilicity and hydrophobicity before hydrogel injection.

The other critical step of the protocol is the removal of bubbles. A large amount of air will dissolve into circulation medium during the experiment due to the T-type connector and micro-peristaltic pump, resulting in bubbles in circulation and greatly affecting the function of endothelial cells. To remove bubbles, a bubble trap chip is introduced before microfluidic sprouting chip. It works based on the high gas permeability of the PDMS membrane. When bubbles get into the trap, they are dispersed by the small and dense grid structure and trapped due to the negative pressure generated by the vacuum pump so that they fail to move forward into the microfluidic sprouting chip. Further, the bubbles transport through the PDMS membrane into the negative pressure hole connected to the vacuum pump and disappear eventually. Even so, great attention should be paid to the formation of bubbles during the experiment. As soon as bubbles are found before microfluidic sprouting chip in the pipeline, stop the micro-syringe pump immediately. Gently flinch the pipeline with the finger to let the bubbles move to bubble trap chip and be removed.

Although the initial microenvironment of neovascularization is partially recapitulated, there are some limitations to this MIEN model. The mechanical microenvironments of endothelial cells such as blood induced shear stress and extracellular matrix stiffness are changing during the neovascularization processes. Before neovascularization, the endothelial basement membrane is still intact with complete barrier function, resulting in high luminal shear stress with low velocity of transendothelial flow and interstitial flow^{8,9}. At the onset of angiogenesis and arteriogenesis, a hallmark event is matrix metalloproteases (MMPs) mediation of basement degradation, which will increase ECs permeability and remodel matrix, leading to changes in mechanical microenvironments such as blood induced shear stress and extracellular matrix stiffness. In the present work, we focus on the initiation of neovascularization so the mechanical environments within the microfluidic sprouting chip are designed to keep stable to simulate the physiological conditions. However, changes of mechanical microenvironments will occur with the ECs sprouting, just like *in vivo*. Besides, similar to many previous studies^{34,53,56}, the present model

takes collagen hydrogel as an extracellular matrix. As we focus on the effect of flow induced shear stress, only one stiffness hydrogel is used. However, considering the important effect of matrix stiffness on cell behavior and neovascularization, different stiffnesses of collagen should be studied and can be achieved by regulating the pH of collagen since the mechanical properties of collagen is depending on its pH⁴⁹. But it is important to note that the hydrogel needs to be thoroughly rinsed with PBS to remove residual acids or bases before cell seeding to prevent damage to the cells. Further, to mimic the complex components of ECM in vivo, various hydrogels such as Matrigel, hyaluronic acid (HA), and fibrinogen etc. should be used in the future to improve the present model. Blood pressure induced cyclic strain is another important hemodynamic force that modulates the morphology and functions of vascular cells⁵⁷. Previous studies have shown that tensile strain enhanced expression of angiogenic factors in human mesenchymal stem cells⁵⁸ and induced angiogenesis via degradation of type IV collagen in the vascular endothelial basement membrane⁵⁹. These results indicated that blood pressure induced strain may affect neovascularization too. The present model focuses on the effect of flow induced shear stress so it isn't applicable to introduce strain as the hydrogel doesn't stick tightly enough to the channel and will fall off when stretched. We will pay attention to overcome this difficulty in future works.

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DISCLOSURES:

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643 644 The authors have nothing to disclose.

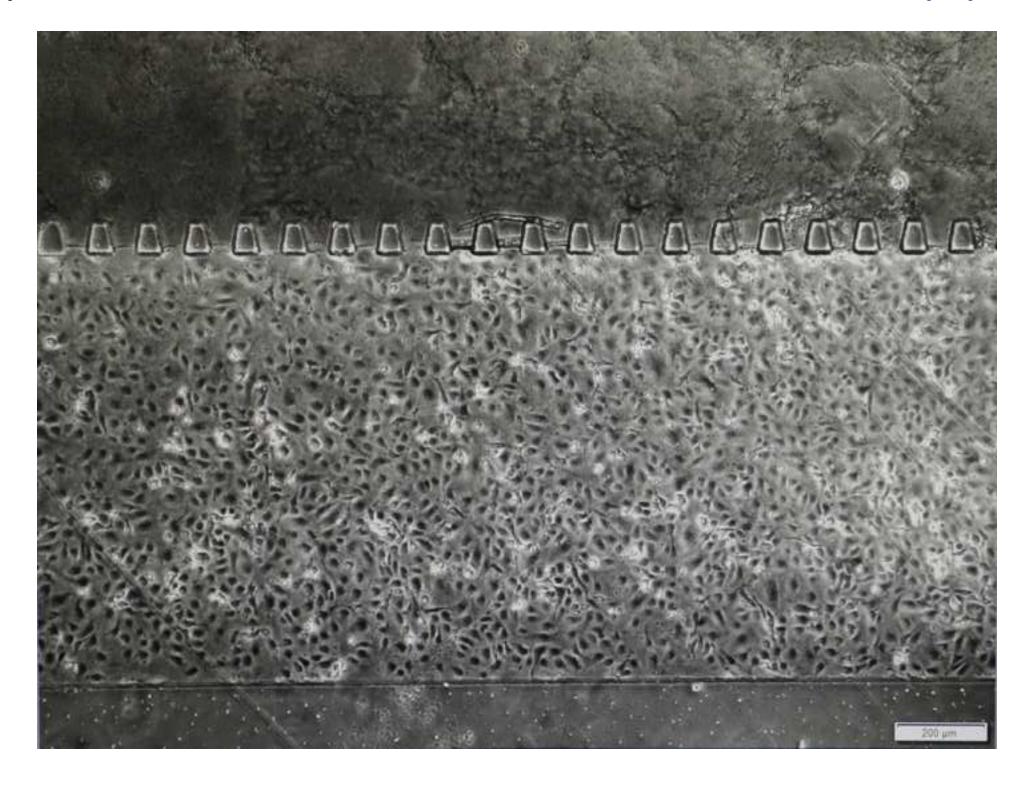
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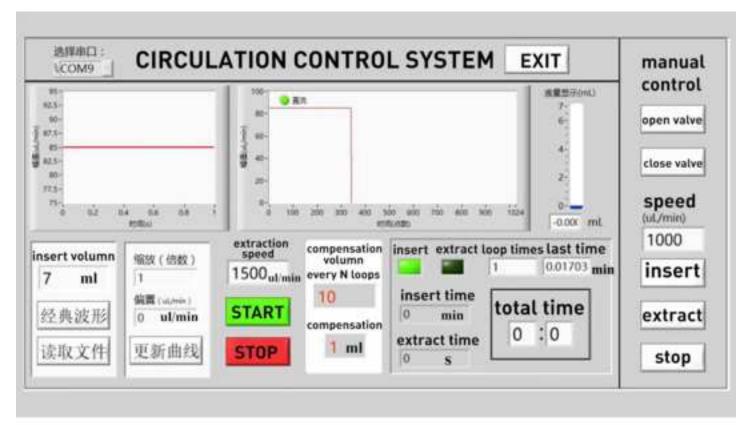
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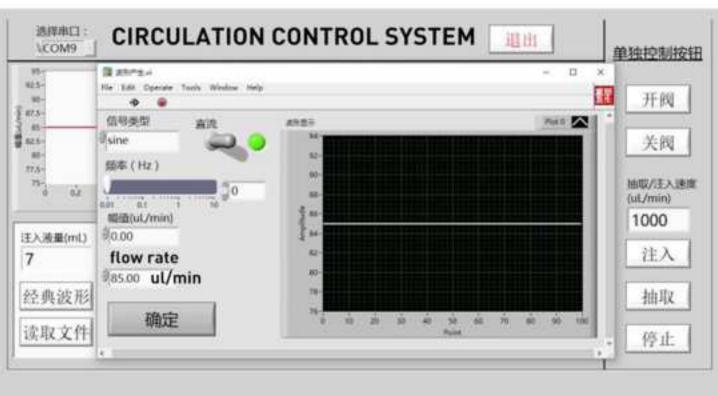
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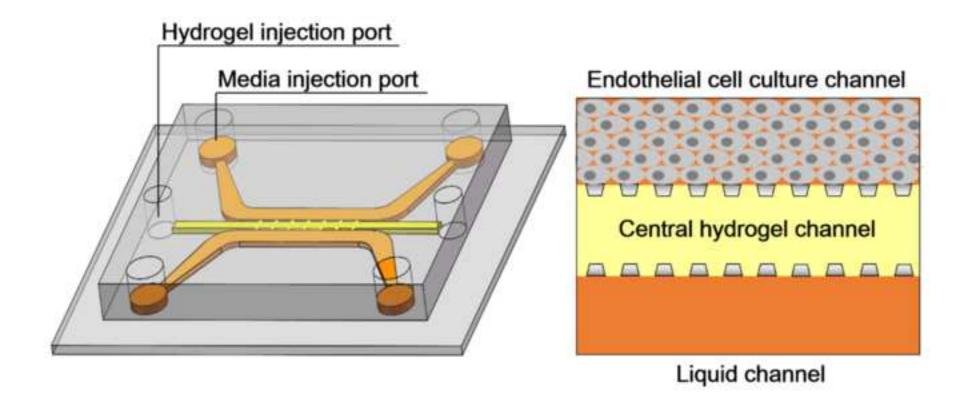
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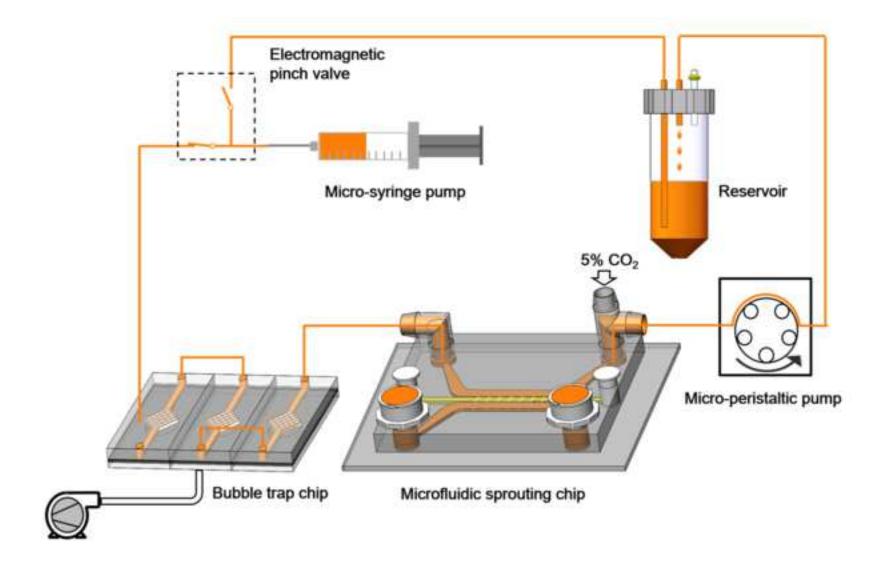
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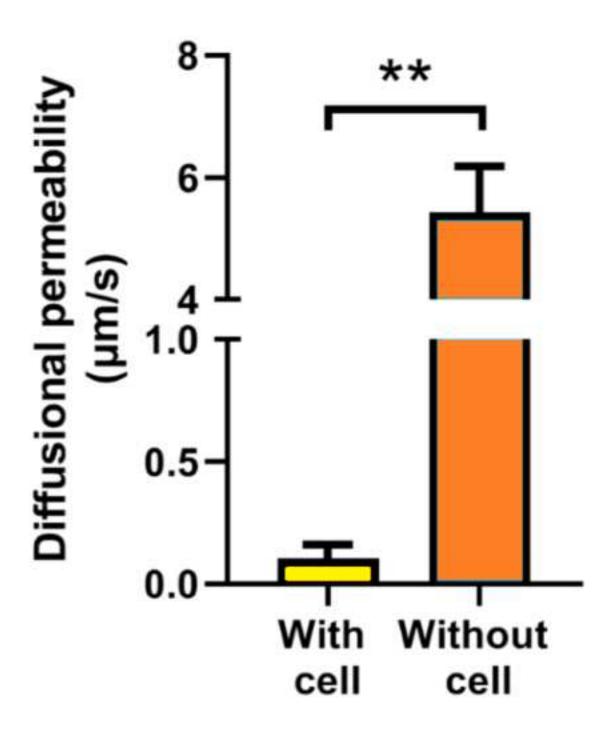


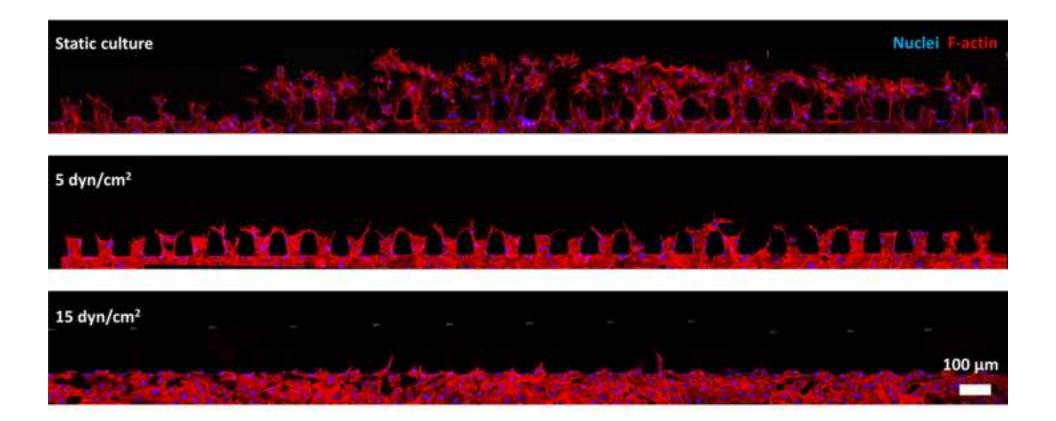


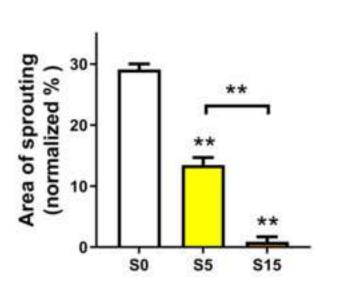


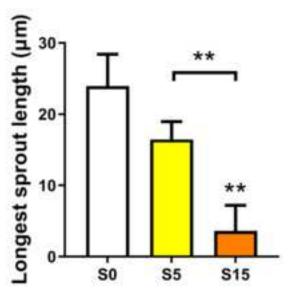


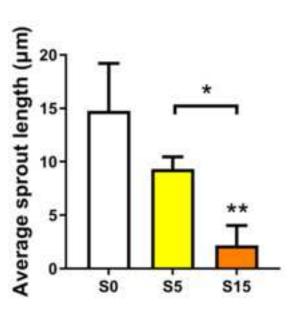












Name of Material/ Equipment	Company	Catalog Number
0.25% Trypsin-EDTA	Genview	GP3108
Collagen I, rat tail DAPI	Corning Sigma-Aldrich	354236 D9542
Electromagnetic pinch valve	Wokun Technology	WK02-308-1/3
Endothelial cell medium (ECM)	Sciencell	1001
Fetal bovine serum (FBS) Fibronectin FITC-dextran Graphical programming	Every Green Corning Miragen	NA 354008 60842-46-8
environment	Lab VIEW	NA
Image editing software Image processing program Isopropanol	PhotoShop ImageJ Sigma-Aldrich	NA NA 91237
Lithography equipment	Institute of optics and electronics, Chinese academy of sciences	URE-2000/35
Methanol Micro-peristaltic pump Micro-syringe pump Oxygen plasma Paraformaldehyde PBS (10x)	Sigma-Aldrich Lead Fluid Lead Fluid MING HENG Sigma-Aldrich Beyotime	82762 BT101L TYD01 PDC-MG P6148 ST448
Permanent epoxy negative photoresist	Microchem	SU-8 2075
Phenol Red sodium salt Polydimethylsiloxane (PDMS)	Sigma-Aldrich Dow Corning	P5530 Sylgard 184
Poly-D-lysine hydrobromide (PDL)	Sigma-Aldrich	P7886
Polytetrafluoroethylene Program software	Teflon MATLAB	NA NA
Recombinant Human VEGF-165	StemImmune LLC	HVG-VF5
Sodium hydroxide (NaOH) Stage top incubator SU-8 developer Trichloro(1H,1H,2H,2H-	Sigma-Aldrich Tokai Hit Microchem	1.06498 NA NA
perfluorooctyl)silane	Sigma-Aldrich	448931
TRITC Phalloidin	Sigma-Aldrich	P5285

Response to Editor

All page numbers and line numbers refer to the file 'Revised Manuscript (marked)'

Response to Editor

Comment 1:

Please move the scripting language from step 8.3/8.4 to a supplemental file.

Response 1:

We moved the codes from step 8.3/8.4 to the supplemental file.

Comment 2:

Please spell out all journal titles.

Response 2:

We corrected the journal to its full name.

Video Comment 1:

Typos:

- 01:08 Reservior should be spelled "Reservoir"
- 01:08 Microfiudic should be spelled "Microfluidic"
- 09:26 Conclution (should be spelled Conclusion)"

Response 1:

Thanks for the editor's suggestion. We corrected the spelling mistakes from the video.

Important correction:

The affiliations of the authors are corrected according to the new rules of the school in this new term and the request of the authors. We corrected the information in both the manuscript and video. In addition, we found that Xiao Liu was lost from the corresponding author list in the manuscript and was added in the revised manuscript.

Supplemental Coding Files

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