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TITLE:

- 2 Sample Preparation and Experimental Design for In Situ Multi-Beam Transmission Electron
- 3 Microscopy Irradiation Experiments

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- **KEYWORDS:**
- In situ ion irradiation TEM; extreme environments; ion implantation; helium bubble; radiation effects; radiation damage

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- **SUMMARY:**
- Sample preparation techniques are outlined with specific considerations for in situ ion irradiation TEM experiments. Ion species, energy, and fluence are discussed with methods for how to select and compute them. Finally, procedures for conducting an experiment are described and accompanied by the representative results.

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- ABSTRACT:
- There is a need to understand materials exposed to overlapping extreme environments such as high temperature, radiation, or mechanical stress. When these stressors are combined there may be synergistic effects that enable unique microstructural evolution mechanisms to activate. Understanding of these mechanisms is necessary for the input and refinement of predictive models and critical for engineering of next generation materials. The basic physics and underlying mechanisms require advanced tools to be investigated. The in situ ion irradiation transmission electron microscope (I³TEM) is designed to explore these principles.

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To quantitatively probe the complex dynamic interactions in materials, careful preparation of samples and consideration of experimental design is required. Particular handling or preparation of samples can easily introduce damage or features that obfuscate the measurements. There is no one correct way to prepare a sample; however, many mistakes can be made. The most common errors and things to consider are highlighted within. The I³TEM has many adjustable variables and a large potential experimental space, therefore it is best to design experiments with a specific scientific question or questions in mind.

Experiments have been performed on large number of sample geometries, material classes, and with many irradiation conditions. The following are a subset of examples that demonstrate unique in situ capabilities utilizing the I³TEM. Au nanoparticles prepared by drop casting have been used to investigate the effects of single ion strikes. Au thin films have been used in studies on the effects of multibeam irradiation on microstructure evolution. Zr films have been exposed to irradiation and mechanical tension to examine creep. Ag nanopillars were subjected to simultaneous high temperature, mechanical compression, and ion irradiation to study irradiation induced creep as well. These results impact fields including: structural materials, nuclear energy, energy storage, catalysis, and microelectronics in space environments.

INTRODUCTION:

The transmission electron microscope (TEM) is widely utilized for its ability to observe specimens at the nanoscale. Early in the development of electron microscopes, microscopists identified in situ TEM as a powerful tool that could be used to directly observe the role of crystal defects, kinetic measurements of reaction rates, and the fundamental mechanisms in dynamic processes ¹. By carefully controlling the environment and directly observing material evolution, insight into fundamental mechanisms can be gained. This knowledge informs predictive modeling for materials response^{2,3}, which is critically important in applications where traditional materials reliability testing is prohibitively difficult; applications where materials are extremely remote, in incredibly hostile environments, in service for exceedingly long times, or a combination of these factors. Radiation environments are one such example where there are significant challenges to conducting experimental studies due to the hazards of radiation areas, handling of radioactive material, and long timelines required for effects.

Space and nuclear reactor settings are both examples of these extreme radiation environments. Materials for nuclear energy can be exposed to high energy neutrons, as well as a spectrum of high energy charged particles. Likewise, in space applications materials can be exposed to a variety of charged particles. Understanding and developing predictive modeling of the resulting material evolution from exposure to these complex and extreme environments requires insight into the fundamental mechanisms occurring at the nanoscale. In situ TEM is one tool for investigating these dynamic nanoscale mechanisms in real time^{4,5}.

In situ ion irradiation experiments in the TEM began in 1961 with the serendipitous emission of O⁻ ions from a contaminated tungsten electron gun filament⁶. Researchers at Harwell were the first to link a heavy ion accelerator to a TEM for direct observation of ion irradiation effects⁷. More recently several facilities have assembled microscopes with multiple attached ion accelerators to enable in situ multibeam ion irradiation experiments including at the Japan Atomic Energy Research Institute⁸, National Institute for Materials Science⁹, Argonne National Laboratory¹⁰, University of Huddersfield¹¹, JANNUS Orsay¹², Wuhan University¹³, Sandia National Laboratories¹⁴, and others¹⁵ including multiple facilities under development. Multibeam ion irradiation can be used to study the synergistic effects that occur due to simultaneous gas generation and displacement cascade damage in materials exposed to complex radiation environments. Elevated or cryogenic temperature TEM stages are often utilized with multibeam irradiation to more closely mimic specific environments, as temperature plays a significant role

in defect evolution. Additionally, mechanical testing stages can be utilized to quantify the role of synergistic effects on mechanical property changes as a function of irradiation dose.

lon irradiation has been used as an accelerated aging technique to simulate the atomic displacement cascade damage that occurs during neutron irradiation in a reactor environment, as the technique can provide many orders of magnitude faster damage rate while avoiding prolonged activation of the target material 16 . The I^3TEM facility at Sandia National Laboratories harnesses two types of accelerators to make possible a wide range of ion species and energies. The high energy ion beam is produced by a 6 MV Tandem accelerator and low energy ions are produced by a 10 kV Colutron accelerator. Au ions up to 100 MeV have been produced in the Tandem, while the Colutron has successfully run gaseous species including H, Deuterium (D), He, N, and $Xe^{14,17}$. A mixed D_2 and He gas plasma can be utilized to perform triple ion irradiation with the heavy ion beam coming from the Tandem, and a mixed D_2 + He beam coming from the Colutron.

Controlled production of ions allows for precise dosing of material to reach a target damage and implantation concentration. When simulating neutron irradiation with ion beam irradiation, the damage dose, in displacements per atom (dpa) can be computed. This value represents the average number of displacements of an atom from its original lattice site position, and is not the same as the total defect concentration. Calculating the total defect concentration requires more advanced simulation tools with the capability to account for recombination effects. The dpa can be calculated using ion irradiation damage models such as the Monte Carlo simulation software Stopping Range of Ions in Matter (SRIM)¹⁸. SRIM can output vacancy distribution, stopping powers, and ion ranges in a target based on the target composition, ion species, and ion energy. This provides information necessary for quantifying ion implantation, radiation damage, sputtering, ion transmission, as well as medical and biological applications.

When considering this tool for investigating the effects of irradiation it is important to design the experiment to take full advantage of the strengths of the technique. The utilization of in situ TEM irradiation creates an ideal scenario to quantify the dynamic evolution of defects created in radiation environments. While this technique provides insight into defect evolution including loop faulting/defaulting reactions and defect-grain boundary (GB) accommodation mechanisms, significant experimental limitations exist in comparing the defect quantification to bulk scale irradiations due to well-known thin-film effects including loss of point defect and defect clusters to the surface^{19,20}.

This article provides novel considerations and procedures on preparation and mounting of samples for in situ multibeam TEM experiments. Also described are experimental design considerations including modeling and geometric considerations specific to the I³TEM facility as well as protocol for beam alignment and beam characterization. A demonstration of the use of SRIM to calculate the energy required for a given depth of ion implantation, and the ion distribution and damage profile is provided. While the modeling methods^{21,22} and some sample preparation methods have been reported previously, the application of this information to experimental design is emphasized here. Representative results from in situ TEM experiments are presented and typical data analysis is also described.

PROTOCOL:

CAUTION: Please consult all relevant material safety data sheets (MSDS) before use. Also, complete relevant training and utilize appropriate precautions for hazards which may include but are not limited to chemicals used, high voltage, vacuum, cryogens, pressurized gasses, nanoparticles, lasers, and ionizing radiation. Ensure authorization and training for use of all equipment. Please use all appropriate safety practices dictated in the operating procedures (radiation monitoring device, personal protective equipment, etc.).

NOTE: All parameters given in this protocol are valid for the instruments and models indicated here:

1. In situ ion irradiation TEM experimental design

NOTE: There are many variables that can be changed resulting in a large potential experimental space. Designing systematic experiments such that they will answer specific scientific questions will result in the most success. First, choose appropriate ion species and energies that will model the system to be emulated.

1.1. Ion species selection

NOTE: Ion interaction with materials is complex and the details are beyond the scope of this document. There exist several publications detailing ion interaction in solids²³, or more specifically with metals²⁴, and semiconductors²⁵. Space radiation environments consist of a spectrum of ion energies and masses, which can be effectively modeled with light and heavy ions. Nuclear systems can be emulated using a combination of heavy ion irradiation and gas implantation. Heavy ion irradiation simulates the displacement cascade damage induced by neutrons and high energy fission or radioactive decay products. He is often generated in nuclear materials by either transmutation reactions or radioactive decay.

1.1.1. Choose an element to implant, based upon chemistry, damage type, and matching neutron spectrum. To minimize chemistry effects due to ion implantation, self-ion irradiation is often utilized, where the ion selected is the same as the material to be examined. Alternatively, doping studies can select specific ions for implantation. Damage type is determined by the kinetic energy of the ions with higher energies producing larger damage. For a fixed energy, light ions can be chosen to produce Frenkel pairs, heavy ions for damage cascades, and heaviest ions for ion tracks²⁶.

1.1.1.1. To simulate neutron damage, choose an ion that matches primary knock-on atom (PKA) displacements with the neutron spectrum of interest²⁷.

NOTE: Not all elements form stable negative ions suitable for use in Tandem accelerators. See Figure 1 for a list of all ions successfully run in the I³TEM facility. For background on accelerator

- operations and a list of 6 MV Tandem compatible elements with stable negative ions please refer to Middleton's cookbook²⁸.
- 178 [Place Figure 1 here]

1.2. Ion energy selection using the stopping and range tables in SRIM

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- NOTE: The Stopping and Range tables provide a quick method for determining the depth of penetration of ions into a material. The stopping power, dE/dx, describes the energy (dE) an ion loses per unit distance (dx) traveled in a solid. The stopping power consists of two components:
- 1) nuclear stopping, the energy lost to elastic collisions with target atoms, and 2) electronic stopping, the energy lost due to interactions with the target atom electrons. The following
- procedure describes the implementation of a typical SRIM table.

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1.2.1. In SRIM software select **Stopping / Range Tables**.

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191 1.2.2. Select the ion to be implanted and the target material. Multiple target elements may be selected for a compound target.

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NOTE: A calculated density is provided but is usually very inaccurate and a value should be entered manually.

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1.2.3. Select **Calculate Table** to see a table of ion energies vs projected range, lateral and longitudinal straggling in the material.

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NOTE: For implantation experiments, the peak stopping range should be within the foil thickness.

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1.2.4. Energies above 6 MV are possible with multiple charge states. Where the ion energy, *E*, is approximately determined by:

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Where M_1 is the mass of the selected ion, M_T is the total mass of the compound in the source $(M_T = M_1 \text{ for single element sources})$, q is charge state, V_T is terminal voltage and V_S is source potential.

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NOTE: Charge states also influence beam current, which will affect fluence achievable and the time of exposure for experiments (see Equations 2, 3).

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215 1.3. Ion fluence and flux selection using SRIM

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NOTE: Verify the penetration depth profile for the energy used in 1.2 by using SRIM. Decide on a target ion concentration (dose, fluence) or damage level based on relevant literature. Damage

- 219 level is often reported in dpa and does not reflect the final number of defects, but is the 220 average number of displacements without accounting for defect annihilation at free surfaces or 221 recombination. Other environmental conditions such as temperature or mechanical load may 222 be applied simultaneously. These may affect the damage and microstructural evolution 223 mechanisms and should be considered. The following is a description of how to use SRIM to 224 calculate damage or fluence. There are alternate methods to calculate damage²², but the 225 method described is widely used and considered simpler and quicker. It is highly recommended 226 that these guidelines are followed for the relevant radiation conditions, and most importantly 227 that the simulation parameters are recorded and reported so that they can be reproduced.
- 1.3.1. In SRIM software, select the ion to be implanted and the target material. Multiple target
 elements may be selected for a compound target. A calculated density is provided but is usually
 very inaccurate and a value should be entered manually.

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- 1.3.2. Select TRIM calculation type: "Ion Distribution and Quick Calculation of Damage" and"Quick K-P" damage model.
 - NOTE: The vacancy.txt method provides a quick approximation of the damage profile that is sufficient for planning most I³TEM experiments. Stoller et al.²¹ detail how to use SRIM to implement the quick Kinchin-Pease equation to determine the dpa per ion per area in metal systems. There are competing arguments for the usage of "quick K-P" vs. "Full Cascade" options^{21,22}, especially in ionic compounds containing elements with different threshold displacement energies. The authors recommend researching each of these methods to determine the most appropriate calculation method for reporting the final dpa in publications, depending on the specific sample type and experimental design.
 - 1.3.3. Set layer thickness the same as the TEM sample thickness (10–150 nm).
- NOTE: The software will automatically divide the depth into 100 bins of equal size, so choosing a larger thickness will cause less accurate binning.
- 250 1.3.4. Set the ion incidence angle to match experimental conditions (typically 60° from normal). 251
- NOTE: The ion beam is nearly normal to the electron beam in the TEM and typically the specimen is tilted towards the ion beam by 30°. See sections 3 and 4 for experimental configuration schematics.
- 1.3.5. Choose a threshold displacement energy from a reputable literature source, such as
 ASTM E521²⁹. Set the lattice and surface energy to zero.
- NOTE: Publications on both modeling³⁰ and experimental work³¹ present threshold displacement energies on various materials. Zero lattice and surface energy are appropriate for most conditions, but for special cases, a value may need to be supplied²¹.

1.3.6. Run the simulation.

1.3.7. Check the VACANCY.txt file for damage events as a function of depth, both VACANACIES
 by IONS and VACANCIES by RECOILS for each depth. This file can be imported into a
 spreadsheet.

NOTE: Using the vacancy.txt file may not be the most accurate method for calculating damage dose and should be considered a quick approximation²¹.

1.3.8. Convert the units from (displacements/ion-Å) to (displacements/ion·cm). Then use the measured ion fluence to determine the dpa or determine the necessary ion fluence for a desired dpa (Equation 2, see section 3.1.5 and 3.2.5 for how to measure fluence). If damage rate (dpa/s) is desired, substitute flux (ions/cm²-s) for fluence.

1.3.9. Calculate the time of exposure necessary for a target fluence.

NOTE: Below are the relationships between these values where *e* is the electron charge and *C* is Coulombs (Equation 3). Some experiments range over several decades of fluence and thus a commensurate range of times with a given flux. For high fluence experiments, maximum flux is desired to minimize experiment time²⁴. Due to the limiting speed of the gate valves and the Faraday cup actuator, low fluence requires a lower flux such that the exposure time can be achieved with sufficient precision: on the scale of seconds. High beam current can result in local heating of the sample which may change the diffusion properties and the observed microstructural evolution. In experiments utilizing high beam current, the sample should be cooled to room temperature and the temperature monitored with thermocouples during the irradiation.

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$$291 \quad \text{PPP PP PPPPPP}(P) = \frac{\frac{\text{PPPPPP}(\frac{\text{ions}}{\text{cm}^2}) \times \text{IPP PPPPPP PPPPPP}(\frac{e}{\text{ion}}) \times \text{PPP PPPPPP}(\frac{e}{\text{ion}}) \times \text{PPP PPPPPP}(\frac{e}{\text{ion}})}{\text{PPP PPPPPPPP}(\frac{e}{\text{p}}) \times 6.24 \cdot 10^{18} \left(\frac{e}{\text{p}}\right)}$$
 Equation (3)

1.4. TEM stage selection

NOTE: Simple ion irradiation experiments can be performed on a single tilt holder. Depending on the material system and properties of interest, however, a variety of holders may be appropriate. It is possible to combine a variety of extreme environment components simultaneously with ion irradiation including conditions such as temperature, gas or liquid environment, and mechanical stress.

1.4.1. Consider the use of cryogenic or heating holders. Temperature plays an important role in the diffusion of atoms. Implantation temperature can influence the type and intensity of damage. Cryo-holders or heating holders can be selected to maintain a desired temperature.

Maintain room temperature with the use of a heating holder running chilled water.

NOTE: For high temperature experiments samples should be mounted to a Mo grid or other thermally stable grids.

1.4.2. Consider the use of double tilt or tomographic holders. Crystal orientation can be important to understand and is needed to obtain two beam condition conducive to quantifying dislocation loops or black spot densities. Double tilt or tomographic holders may be used for these cases. This would also be useful for examining radiation induced phase changes.

1.4.3. Consider the use of environmental holders to expose the material to gas or liquid in situ. Specimen preparation for this type of experiment varies, can be very difficult, and is beyond the scope of this document³².

1.4.4. Consider the use of stages specialized for mechanical testing including tension, compression, bend, fatigue, and creep.

NOTE: Specific sample preparation is required for these types of experiments and is beyond the scope of this document³³⁻³⁶. Now that the ion species, ion energy, and target fluence have been determined, and specific holders for additional environmental complexity have been considered, the next step in designing ion irradiation experiments is preparing specimens for TEM. Careful preparation of the specimen is required to satisfy the geometric constraints for in situ ion irradiation TEM experiments. Several sample preparation methods are described below.

2. Preparation of thin sample and mounting on TEM grid

NOTE: There are many ways to prepare a sample for TEM. The most appropriate method depends on starting sample geometry, material, and features of interest. For an extensive list and descriptions of preparation methods please refer to the sample preparation handbook for TEM³⁷. Below are described three common methods. For magnetic materials a bonding method should be applied so the films or particles do not come off when subjected to the magnetic field in the TEM. Insulating substrates (i.e., oxides) should be avoided to minimize electrostatic expulsion due to ion beam induced charge.

2.1. Drop casting of nanoparticles

NOTE: This is the most straightforward method for TEM sample preparation for nanoparticles with diameter less than 200 nm. Several different support materials can be used including lacey carbon, polymer, and silicon nitride membranes. These materials may interact differently with the nanoparticles due to ligand interactions. Select whichever substrate results in well dispersed nanoparticles.

2.1.1. Disperse nano-particles into a solvent such as alcohol, deionized water, or other
 combination until well mixed. Sonication may be used to break up additional agglomerates. The
 fluid concentration can be used to control the nanoparticle density on the grid.

2.1.2. Use a Pipette to deposit dispersed particles onto the top side of a supported TEM grid.

NOTE: Make sure the support side of the grid is facing upwards, so the nanoparticles stick on the top side of the grid. It is possible to take advantage of the capillary effect which drags the nanoparticles as the droplet dries. An off-center drop will result in a lower density of nanoparticles in the central irradiation area.

2.2. Thin film float-off

NOTE: This method requires a thin (<100 nm) film deposited on a dissolvable substrate such as salt or photoresist. A small portion of the sample is cleaved and placed into a solvent. As the substrate dissolves in the solvent, the thin film separates from the substrate and floats to the surface of the solution where it can be scooped onto a TEM grid.

2.2.1. Prepare 50 mL of solvent solution in a Petri dish.

NOTE: The solvent depends on the substrate for the thin film. NaCl substrates are common with water being the solvent. Alcohol can be added to the solution to change the surface tension. Too much alcohol will often cause the sample to sink, and too little alcohol will increase the surface tension making it difficult to transfer the film to the grid.

2.2.2. Cleave or cut the substrate into approximately 1.5 mm × 1.5 mm sections.

NOTE: The edges of the film are usually lower quality and should be avoided when possible.

2.2.3. Using tweezers, insert the substrate, with film facing up, into the solution at an incident angle of about 30° (Figure 2a). Repeatedly retract and insert slowly until the film floats free (Figure 2b,c). The substrate can be set aside.

2.2.4. Insert the TEM grid into the solution and bring below the film. Slowly lift the grid under the film until film is centered over grid. Quickly lift the grid out of the solution and the film will attach (**Figure 2d**).

NOTE: If film is not well centered reinsert the grid and film into the solution to re-float the film and center as necessary. Be aware that the film can fold back on itself.

[Place Figure 2 here]

389 2.3. Focused ion beam milling

NOTE: Most bulk materials can be prepared by focused ion beam (FIB) milling and information detailing this process can be found in the handbook for TEM sample preparation³⁷. FIB milling is a time consuming and involved process compared to the methods mentioned previously but is very short and easy compared to traditional hand polishing methods of preparing TEM specimens from bulk samples. It also has the advantage of high degree of control over the site which allows for selection of area of interest to investigate, such as boundaries or defects. The foils produced by FIB have residual ion irradiation damage induced by the ion beam milling process that will convolute quantification of the damage induced by the in situ irradiation³⁸.

2.3.1. Prepare the lift out. A variety of lift out strategies can be used to produce site-specific TEM foils in different geometries. For detailed methods please refer to publications for preparing samples in geometries such as: cross sectional³⁹, plan view⁴⁰, crack tips⁴¹, nanopillars⁴², atom probe needles⁴³, etc.

2.3.2. Mount the foil. Ex situ lift outs can be placed on top of TEM grid similarly to thin films (**Figure 3a**). For specimens welded to a grid, the foil should be welded on the tip of a post on the face of the grid to avoid shadowing effects (**Figure 3b**). Avoid mounting in the V posts (**Figure 3b**: left and right).

2.3.3. Perform a final polish to the lamella. Standard FIB thinning will result in ion beam damage to the specimen. This damage can be minimized by flush polishing at a very small glancing angle and by gentle milling with a low accelerating voltage. Alternatives to traditional final thinning via Ga^+ ion beam include flash electropolishing^{44,45} and ion milling with Ar^{+46} .

2.4. Electro polishing

NOTE: This is often the most preferred method for preparing single phase metallic specimens for in situ ion beam irradiation experiments from bulk material. It avoids the damage caused by FIB milling and traditional polishing techniques. However, the electrolyte solution, electric potential, and time for polishing are material specific and these parameters may be difficult to determine.

[Place Figure 3 here]

3. Ion beam conditions and alignment

3.1. Tandem accelerator

NOTE: The Tandem accelerator is best suited for high energy ions 800 keV - 100 MeV. Sources of negative ions by cesium sputtering (SNICS) are frequently used to produce energetic metal ion beams and its operation is outside the scope of this document²⁸. Adjustments and considerations for in situ TEM experiments are described below.

- 3.1.1. Align the ion beam inside the TEM with steering magnets, bending magnets, and lenses so that irradiation events can be observed in situ. Perform final ion beam alignments by using a camera to view ion beam induced luminescence (IBIL) on a quartz-tipped TEM sample holder.
- 438 3.1.1.1. Align the ion beam to be coincident with the cathodoluminescence produced by the electron beam with electron beam objective lens power matching that used in the experiment.
- 3.1.2. Insert the Faraday cup upstream from the TEM to capture the ion beam, and take a reading to measure the beam current. Beam current measurements are necessary to calculate the fluence (Equation 3).
- 3.1.2.1. For additional accuracy in the beam current measurement, insert a TEM holder equipped with a Faraday stage to measure the ion beam current in the specimen area of the TEM.
- 3.1.2.2. If current needs to be monitored in real time, use the beam profile monitor (BPM).
 Power on the BPM then monitor the oscilloscope read out to perform current measurements.
 The BPM works by regularly chopping the beam which results in temporal distortion of the beam and is a qualitative measure of the beam current.
- NOTE: The ion beam current can drift so checking its stability throughout the experiment is advised.
- 3.1.3. Measure the beam area using a burn spot. Burn spots can be used to confirm alignments in 3.1.1.
 - 3.1.3.1. Mount a piece of clear adhesive tape onto a single-tilt TEM specimen holder flat plate tip and expose to the electron beam and ion beam. Remove the tape and place onto a white background.
 - 3.1.3.2. To determine the area, photograph the burn spot with a ruler and import into an image processing software such as ImageJ⁴⁷. Together with beam current, the beam area measurement can be used to determine the ion flux (Equation 2).
 - 3.1.4. Insert a calibration sample to visualize beam damage, which should appear as black spot contrast in kinematic bright field imaging conditions. Typically, Au or CuAu are chosen due to their readily apparent black spot formation and ease of sample preparation⁴⁸.
 - 3.2. Colutron accelerator

NOTE: The Colutron accelerator utilizes a gas-fed hot filament ion source⁴⁹. It is possible to accelerate multiple gas species simultaneously, however, the mass to charge ratio of the two ion species must be equal in order for the bending magnet, steerers, and lenses to act identically; for example, ⁴He²⁺ and ²D¹⁺.

3.2.1. Perform SRIM calculations as described in section 1.2 to obtain the desired gas implantation energy.

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NOTE: The necessary bending magnet strength depends on the mass of the ion, its charge state, and the accelerating voltage. If the gas species has multiple isotopes, selecting the one which is most abundant will result in highest beam current. Also note that if the Tandem is active, this bending magnet will also act on its beam; additional corrections for the tandem will have to come after the Colutron beam is aligned.

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3.2.2. Steer the ion beam such that it is coincident with the electron beam, as described in step 3.1.1.

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491 3.2.3. Measure the beam current as described in step 3.1.2.

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493 3.2.4. Estimate beam area using a burn spot, as described in step 3.1.3.

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NOTE: This step can be performed simultaneously with the measurement of the ion beam from the Tandem accelerator. However, if the beam current from the Colutron accelerator is too high compared to the beam from the Tandem (> 3 orders of magnitude) it will cover up the signal and the measurements should be made separately.

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3.2.5. Perform final adjustments to steer the beam onto the TEM specimen as described in step 3.1.4.

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4. TEM loading and imaging conditions

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4.1. Specimen loading and geometric concerns

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4.1.1. Load grid onto the holder such that the specimen side of the grid is facing up and the grid is oriented to prevent shadowing effects when titled towards the ion beam (**Figure 4a,c**).

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NOTE: **Figure 4b,d** depicts a schematic of the ion beams path and electron beam path in the irradiation configuration where the effective experimental area is highlighted.

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4.1.2. Check for shadowing effects using an optical microscope. Tilt the holder 30° in the positive X direction as shown in **Figure 4a,b**. The overhead view will be parallel to that of the electron beam. Tilt the holder 60° in the negative X direction where the overhead view will be parallel to that of the ion beam. If the area of interest of the specimen is not visible in both orientation, there is a shadowing issue and the specimen must be moved.

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519 NOTE: For some holders the bottom of the stage has fewer shadowing issues and thus tilting to 520 negative 30° such that the ion beam strikes the bottom side of the sample may be optimal 521 (Figure 4d).

523 4.1.3. Mount the specimen onto a TEM holder following the manufacturers guidelines for the specific holder. Load the holder into the TEM to begin the pump cycle. Wait for vacuum to stabilize and insert the holder.

NOTE: When loading and unloading holders in the TEM, the valve to the beamline should be closed to prevent any loading induced vacuum crashes in the TEM from affecting the beamline.

4.1.4. In the TEM control software, load the most recent alignment file for the accelerating voltage being used. Manually refine the alignments for the condenser lens and aperture, gun tilt and shift, and the objective lens.

4.1.5. Find a region of interest on the specimen and adjust imaging conditions as described by Jenkins and Kirk⁵⁰ for the type of analysis to be performed. Use brightfield kinematic conditions to image damage events.

NOTE: For high Z number materials such as tungsten, an additional condenser lens may be engaged for additional brightness.

NOTE: Low Z materials can be displaced by high energy electrons resulting in knock-on damage from the electron beam that may convolute the damage caused by the ions⁵¹. Using a low dose electron beam and limiting exposure to the specimen as well as using low dwell time scanning TEM will help to mitigate this.

4.1.6. Tilt the holder the maximum safe distance (30° for most holders) up to 81° towards the ion beam.

4.1.7. Apply any additional stressors such as heating, cooling, environmental, mechanical, etc. using the manufacturer recommended procedures for specific to the chosen TEM holder.

NOTE: For high magnification work, allow time for stage to stabilize so drift is not significant. Applied stressors may cause the specimen to deform as well.

4.1.8. Open the TEM ion beam valve and remove the Faraday cup to expose the experimental specimen to ion irradiation. Pause exposure by inserting the Faraday cup and closing valves to the beam line. The Faraday cup should be inserted before closing the TEM valve to prevent damage to the valve.

NOTE: The gun pressure in the TEM should be monitored such that it does not exceed the manufacturer-specified threshold for safe operation levels. It may be necessary to halt exposure to allow vacuum to recover if sample or stage is producing significant outgassing during ion beam exposure.

4.1.9. Record images or videos to document the evolution of the microstructure.

4.2. Additional imaging modes

4.2.1.To map relative orientations of grains, use automated crystal orientation mapping (ACOM), a technique which allows for the identification of the crystallographic orientation of all crystallites with sizes as low as 10 nm. Software systems automate the collection of diffraction patterns with a precessed beam which are indexed resulting in an orientation map⁵².

4.2.2. For ultrafast events, use the high-speed deflector. It is a magnetic lens that deflects projected electrons into different quadrants of the camera at fast rates effectively increasing frame time by an order of magnitude. It can be used to capture events that occur in the microsecond time scale in a single frame⁵³.

4.2.3. Perform electron tomography by capturing a tilt series of the specimen and subsequently perform reconstruction with software. This reveals the three-dimensional structure of the specimen and can be used to analyze volumetric distributions⁵⁴.

4.2.4. Make electron holography measurements by capturing a through-focus series. This measurement can be used to distinguish voids, bubbles, and nanoparticles⁵⁵.

4.2.5. Use weak beam dark field to view dislocations and damage caused by the ion beam. Two-beam condition for a single crystal is used to measure dislocation character and density⁵⁰.

REPRESENTATIVE RESULTS:

In situ ion irradiation TEM experiments have been conducted on several material systems and with several different methods of specimen preparation^{14,32,56-75}. Below are a few selected systems that demonstrate this variety. Sample preparation methods include nanoparticle dropcasting, thin-film float off, cross-sectional FIB liftout on half-moon grid, push-to-pull foils, and nanopillars.

Highlighted here is an experiment on the effects of single ion strikes on Au nanoparticles (NPs)⁶⁰. The number density of particles in the irradiation window was controlled by taking advantage of the capillary forces that pull NPs along as a droplet dries. By dropping off center, the droplet pulls NPs towards the edge of the disc as it dries. The active mechanisms for damage can be highlighted by taking the difference before and after an event (**Figure 5**). The measurements reveal several mechanisms for damage induced by single self-ion irradiation including creation of surface craters, sputtering, filament formation, and particle fragmentation where the types of damage depend on ion energy. Filament formation is seen at lower ion energies, whereas cratering, sputtering, and particle fragmentation are observed at high ion energies. These different energy regimes can be used to investigate the effects of the electronic and nuclear stopping powers.

[Place Figure 5 here]

Nanocrystalline thin films of Au were prepared for in situ multibeam TEM experiments. The samples were deposited by pulsed laser deposition onto NaCl substrates then floated off in deionized water onto Mo TEM grids. The samples were annealed in a vacuum furnace at 300 °C for 12 h to relax the as-deposited metastable nanocrystalline structure resulting in polycrystalline gold with ultrafine grain size.

In this study, 2.8 MeV Au⁴⁺ ions are used to simulate neutron irradiation. The energy is chosen based on SRIM modeling to result in peak damage within the film thickness (**Figure 6a**). Simultaneous 10 keV He⁺ simulates the production of α -particles from neutron-radiation induced nuclear reactions. The He ion energy is chosen such that the ions are implanted within the foil thickness rather than passing through (**Figure 6b**).

[Place Figure 6 here]

The material was then irradiated by Au ions and damage was observed with respect to fluence. The microstructure developed defects induced by the high energy ions (**Figure 7**). With increasing time of exposure and thus fluence, the damage increased linearly. At high doses the concentration of damage sites is too high to reliably quantify.

[Place Figure 7 here]

To explore the effects of multiple beams interacting with the material at the same time, double and triple ion beam irradiation is then performed on Au (Figure 8). Cavity nucleation, growth, and evolution are measured.

To explore irradiation induced creep in Zr, a microelectromechanical system (MEMS) device was fabricated by sputter depositing Zr thin films on silicon-on insulator wafers followed by photolithographic patterning and subsequent deep reactive ion etching. **Figure 9** shows the free standing Zr specimen and the Si push-to-pull test frame which enables in situ tensile testing. 1.4 MeV Zr ions were used to irradiate the specimen under load to determine irradiation creep response in Zr. By conducting the experiment in a TEM, dynamic mechanisms at the nanoscale can be observed. Measurements reveal a texture change as well as a lengthening of the specimen. Volumetric swelling was not expected due to the thin foil specimen geometry, room temperature conditions, and low levels of irradiation damage. This is confirmed by the lack of observed bubble and cavity formation.

[Place Figure 9 here]

 Additional mechanical stressor states can be applied simultaneously during in situ ion irradiation TEM experiments. **Figure 10** shows work on high temperature irradiation induced creep of Ag nanopillars⁶⁷. This utilizes a picoindentor to apply a controlled stress to a TEM specimen. Pillars were prepared from 1 μ m thick Ag film grown on Si by FIB milling. The pillars were irradiated with 3 MeV Ag³⁺ ions. The specimens were heated with a 1064 nm laser beam coincident with both the ion beam and electron beam. The results of this study show that combined irradiation and

temperature result in orders of magnitude faster creep rate than room temperature irradiation and high temperature thermal creep.

[Place Figure 10 here]

 Considerations for the preparation of nanopillars for shallow ion irradiation has been described in depth by Hosemann et al.⁷⁶. One of the key factors to consider is the shape of the nanopillar. At this small scale any deviation from ideal geometry can have a large impact on the mechanical performance. A rectangular prism tip is much better than a cylindrical tip due to tapering of the tip in annular milled geometry.

These representative results demonstrate a range of material systems, preparation methods, and complex environments that are possible with in situ ion irradiation TEM. In each case careful sample preparation and planning of experimental parameters are critical to extract meaningful data. Further detail on these considerations is discussed below.

FIGURE LEGENDS:

Figure 1: Ions run to date (highlighted in blue), charge states, and energy ranges in I³TEM.

Figure 2: Thin film float-off. Schematic showing (a) the insertion of a section of thin film, deposited on soluble substrate, into a solvent solution, (b) a cross sectional view of floating off the thin film by dissolving the adhesion layer of substrate, (c) a cross sectional view of thin film free floating on solution by surface tension, and (d) using TEM grid to lift the film from the solution.

Figure 3: Schematic showing TEM grids with specimens mounted on upper face to prevent shadowing. Grid with lacey carbon or thin film (a), half-moon grid with FIB lift-out welded to tip (b).

Figure 4: TEM loading and imaging conditions. Overhead view of TEM holder with electron beam direction into the page with holder tilted 30° in positive X (a) and negative X (c). Cross sectional view down the axis of the holder with electron beam (green) and ion beam (blue) highlighted with holder tilted 30° in positive X (b) and negative X (d) for bottom side illumination of the ion beam. Highlighted area where both the electron beam and ion beam are not shadowed.

Figure 5: Effects of single 46 keV ions in NPs of decreasing size. Note that the magnification is similar for all micrographs. Each pair of micrographs is separated by 1 frame, about 0.25 s here. (a–c) A single ion strike in a 60 nm NP created a surface crater, marked by the white arrow. Panel (c) shows the difference image highlights the change between (a) and (b); features present only in (a) are dark and newly formed features present only in (b) appear light. (d–f) A single ion creating a crater in a 20 nm NP. Panel (f) shows the difference image of (d) and (e). This figure has been modified with permission from Cambridge University Press⁶⁰.

Figure 6: SRIM modeling. SRIM calculated (a) displacement and (b) concentration profiles as a function of depth for Au irradiated with various ion species. The total dpa profile (D + He + Au) is indicated by purple stars in (a). Lines of fit are a guides to the eye. This figure has been modified with permission from MDPI 17 .

Figure 7: TEM images showing damage spots. TEM images from in situ 2.8 MeV Au⁴⁺ irradiation into a Au foil using dose rates of 9.69×10^{10} (**a–c**) and 9.38×10^8 ions/cm²·s (**e–g**), at fluences of 4.85×10^8 , 1.45×10^{12} and 3.39×10^{12} ions/cm². (**d,h**) show linear increases in number of damage spots with time. All TEM images were taken at the same magnification. This figure has been modified with permission from MDPI¹⁷.

Figure 8: In situ TEM images showing cavity growth. In situ TEM images showing cavity growth as a function of time due to (a–d) double ion irradiation with 5 keV D + 1.7 MeV Au and cavity formation and collapse as a function of time due to (e–h) triple ion irradiation with 10 keV He, 5 keV D and 2.8 MeV Au. Dashed circles highlight the cavity of interest in each image. This figure has been modified with permission from MDPI¹⁷.

Figure 9: In situ mechanical testing. (a) SEM image of the push-to-pull device with Zr tensile sample location highlighted. (b) Low-magnification TEM image of the device from (a). (c) Higher-magnification bright-field TEM image of the nanocrystalline Zr microstructure in the test region. This figure has been modified with permission from Springer Nature⁷⁵.

Figure 10: Radiation-induced creep. Radiation-induced creep rate versus pillar diameter at 75 and 125 MPa loading stresses (left), selected frames from video recording of in situ TEM radiation induced creep in Ag nanopillar irradiated by 3 MeV Ag ions (right). This figure has been modified with permission from Elsevier⁶⁷.

DISCUSSION:

The procedures described in this document are specific to the I³TEM facility at Sandia National Laboratories, however the general approach can be applied to other in situ ion irradiation TEM facilities. There is a facilities group called the Workshop On TEM With In situ Irradiation (WOTWISI), that holds biannual meetings to discuss ion accelerator electron microscopes. There are several facilities in Japan including at the Japan Atomic Energy Research Institute (JAERI)⁸, and the National Institute for Materials Science (NIMS)⁹. Another facility capable of in situ ion irradiation is the Microscope and Ion Accelerator for Materials Investigations (MIAMI) facility at the University of Huddersfield⁷⁷. CSNSM-JANNUS Orsay facility⁷⁸ equipped with a FEI Tecnai G² 20 TEM working at 200 kV and coupled with the IRMA ion implanter. IVEM-Tandem Facility at Argonne National Lab is a Nuclear Science User Facility¹⁰. These facilities integrate ion accelerators differently which results in unique angles of intersection of the ion beam and electron beam. Some of the Japanese facilities introduce the ion beam at 30-45° from the electron beam, ANL and MAIMI similarly at 30° JANNUS at an angle of 68°, and I³TEM and Wuhan university have ion beams normal to the electron beam.

Depending on the material and starting form of the sample a variety of techniques can be used to prepare a specimen for TEM. The specimen needs to be sufficiently thin (less than about 100 nm) to be imaged in a TEM. Several methods for specimen preparation can be found in the handbook of TEM sample prep methodologies³⁷. Of greatest ease are nanoparticles which can readily be drop cast. Thin films deposited on soluble substrate are also quite easy to prepare (Figure 2). Bulk metallic material can be prepared by polishing thin followed by punching through with jet polish where the area around the hole is thin enough for TEM viewing. The focused ion beam (FIB) lift out method is a well-known method for preparing a variety of materials for TEM and has been described in depth previously^{39,79,80}. One primary advantage of the technique is the ability to selectively examine sites such as grain and phase boundaries. Another advantage is the variety of possible sample geometries including: foils, nano tension, nanopillars, and atom probe needles for additional stress environments or correlative studies. The drawback for FIB prepared samples for in situ ion irradiation experiments is that damage induced by the FIB process convolutes damage accumulated during the experiment making it difficult to determine quantitative observations. Biological or polymer samples can be prepared via cryo-FIB or cryomicrotomy, however these processes are not detailed here.

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When planning ion beam implantation or irradiation experiments it is necessary to consider a number of important parameters for the ions. Penetration depth, flux/fluence, and radiation damage are variables that are often controlled when investigating effects of radiation. These parameters are modeled using a variety of simulation techniques. Stopping Range of Ions in Materials, SRIM, is a Monte Carlo simulation written to calculate ion deposition profiles in materials exposed to energetic beams of ions^{21,81}. An alternative to SRIM is the Robinson model⁸² which uses a variety of functions to model the various physics of high energy ion interaction in materials. Another alternative is a model developed for single event effects in aerospace applications which can be adapted for use in ion beam experiments⁸³. SRIM uses the Kinchin-Pease⁸⁴ equation to model the displacement of atoms by radiation. The software is easy to use, and a range of ions, target elements, and ion energies can be quickly calculated with a variety of useful outputs. However, the software is limited in choice of models to use and since it is a Monte Carlo program takes a large number of iterations, and proportionally longer time to run the larger the simulation. The Robinson model utilizes a modified version of the Kinchin-Pease equation⁸⁴ that has a higher agreement with experimental results, however, it is more difficult to use. Because of its widespread adoption and ease of use, methods for using SRIM were applied here and have generally become the industrial standard.

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One of the primary limitations when considering multibeam in situ TEM is the sample geometry. Because of the nature of TEM as a projection imaging technique and the linear ion beam, shadowing of the electron beam or ion beams can affect the experiment. Shadows from the electron beam and ion beam can be formed from the sample stage, mounts, and even other parts of the sample. To avoid shadowing of the sample by the stage, most stages have a tilt limitation between 25° and 40°. More consideration must also be taken to account for geometries where the sample may shadow itself or be shadowed by the TEM grid. For this reason, when mounting the specimen, take care to mount such that there is the lowest possibility of shadowing. For FIB

mounting samples on post grids this means attaching to the end of the post at the furthest out and highest point.

For experiments involving simultaneous irradiation by multiple ion species, there are limitations. Because the different ion species are being produced by different accelerators or sources the second beam must be bent by the magnet into the path of the first. This bending angle for the described instrumentation is about 20°. There must be a high ratio of beam rigidity for the bending to result in colinear beams. Beam rigidity (B_ρ) is defined by total momentum divided by total charge, it can be calculated by:

$$\mathbb{P}_{\mathbb{P}} = \frac{\mathbb{P}}{\mathbb{P}} = \mathbb{PP} \frac{\mathbb{P}_0 \mathbb{P}}{\mathbb{P}}$$
 Equation (3)

Where p is momentum, q is charge, θ is particle bending velocity proportionality ($\theta = v/c$), m_0 is the rest mass of the ion, c is the speed of light, and γ is the relativistic Lorentz factor:

$$\mathbb{Z} = \frac{1}{\sqrt{1 - \mathbb{Z}^2}}$$
 Equation (4)

This means that for multibeam experiments, it is best to use high energy heavy ions and low energy light ions such as Au and He respectively. If multiple beams are being produced by the same accelerator, they must have the same mass/energy ratio, for example $^4\text{He}^+$ and $^2\text{D}_2^+$. Imaging conditions can also affect the ion beams. The objective lens magnetic field in high magnification imaging modes can be strong enough to bend the path of ions. Keep in mind the type of analysis that is desired when aligning the ion beams.

Contrast in TEM can arise from differences in thickness, phase, crystal order, and chemistry. Depending on the feature to be examined, there are several different types of contrast and imaging conditions that should be considered. Understanding the mechanisms behind diffraction contrast and phase contrast is useful. Understanding how to manipulate the electron microscope to achieve two-beam dynamical, bright-field kinematical, and weak-beam dark-field imaging conditions will also be useful. These are described in detail in Jenkins and Kirk, 2000⁵⁰.

To analyze dislocations, multiple diffraction patterns at different angles must be indexed to determine the reciprocal space lattice vector (g). Two beam imaging conditions can then be used to determine the Burgers vector of the dislocations (b). In weak beam dark-field, the dislocations can be imaged with higher resolution and contrast. This method is applied when there is a high density of dislocations or many partials. To calculate volumetric dislocation density, the thickness of the foil must be measured precisely in the area of interest. This can be done using a technique such as electron energy loss spectroscopy or convergent beam electron diffraction. For low angle grain boundaries, the dislocations in the boundary can be distinguished as a network under two beam dynamical conditions. For high angle grain boundaries, one grain is imaged in two beam dynamical conditions and the other in kinematical conditions. Twin boundaries can be characterized similarly. Fresnel imaging conditions are used to visualize gas filled bubbles and voids. Small cavities are more visible when the image is slightly out of focus and in kinematical diffraction conditions. Underfocused conditions are used to determine real diameter. Bubbles can also induce strain fields for which values can be estimated in the case of small bubbles. Automated Crystal Orientation Mapping (ACOM) is used to map several grains and their orientation similar to Electron Back Scatter Diffraction (EBSD) in the scanning electron microscope (SEM). It is best if crystals are through thickness to avoid interference from overlapping diffraction patterns.

It is possible to conduct experiments with other external stressors such as temperature and mechanical stress. The sample preparation and experimental considerations are much the same as for the multibeam experiments. Care needs to be taken in ensuring that the heating method and temperature range is appropriate for the material. Geometry must also be considered to avoid shadowing effects. The special holders for heating or mechanical testing will have specific geometric constraints and their specifications must be consulted ¹⁴. Combinations of these stressors are also possible. In situ mechanical testing requires additional sample preparation to the appropriate geometry. There are specialized stages for experiments to test mechanical performance in various loading conditions such as: tension, compression, bend, fatigue, and creep. In situ heating can be performed both while irradiating and after irradiation for anneal studies. MEMS based, or conductive heating stages can be used to control temperatures up to 1000 °C. Higher temperatures can be achieved using an in situ laser to heat samples to a few thousand degrees Celsius ³³. Samples can be subjected to different environments with in situ holders. This includes various gases, liquids, and even corrosive environments.

In summary, in situ multibeam TEM experiments have the capability to emulate extreme environments and observe the microstructure and material evolution in real time at the nanoscale. The insight into the fundamental mechanisms governing dynamic processes gained from these experiments can help inform predictive models that pave the way for design of next generation materials. It is important to prepare samples as described to insure the best chance for a successful experiment.

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DISCLOSURE:

The authors have nothing to disclose.

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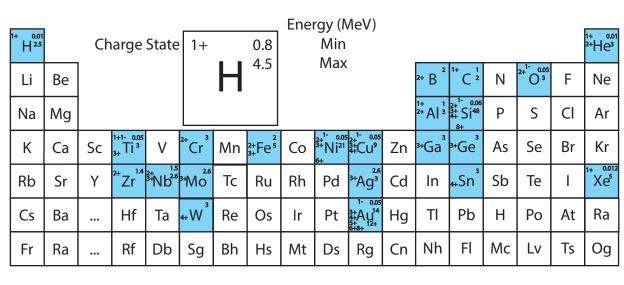
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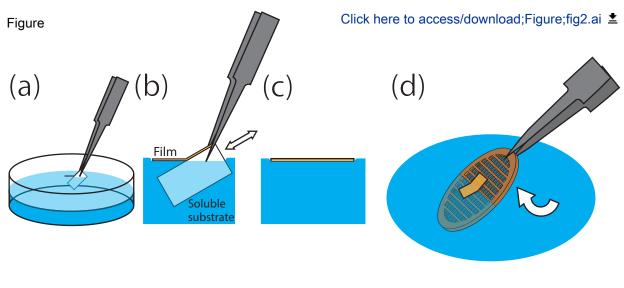
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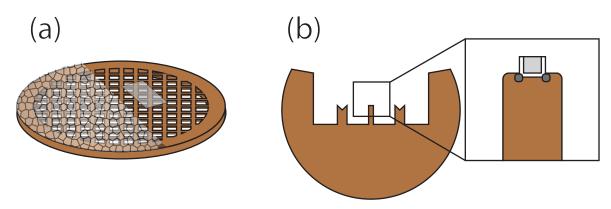
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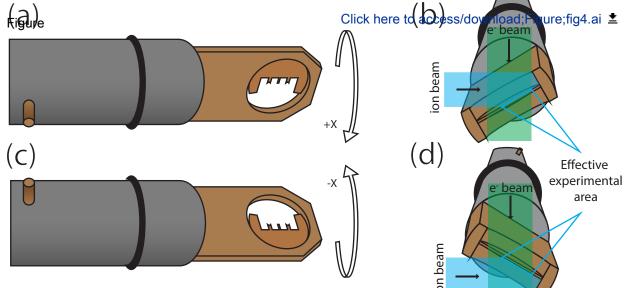


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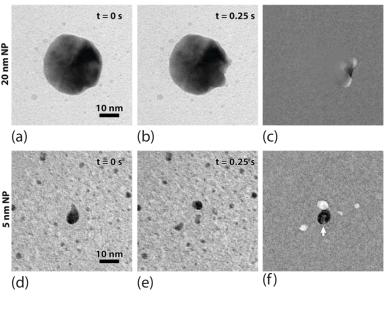


Figure

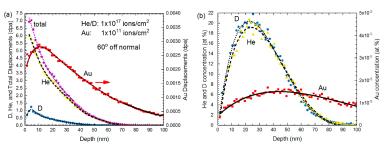




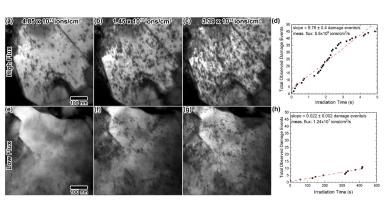
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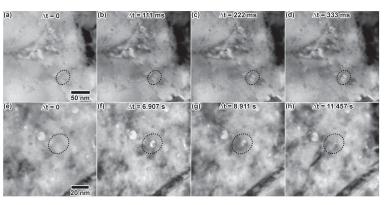






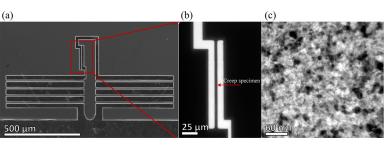




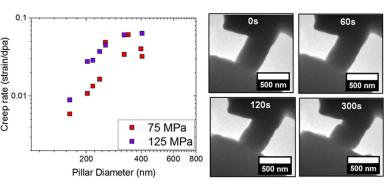












Comments/Description

10 kV ion accelerator
Cu Omniprobe Lift-Out Grid with 4 posts
Cryogenically cooled double tilt TEM holder
Resistive heater equipped double tilt TEM holder
Modified transmission electron microscope for in-situ ion irradiation
70 % v/v isopropanol
Mo Omniprobe Lift-Out Grid with 4 posts

60 mm diamter 15 mm height petri dish

Picoindenter TEM Stage

Dual beam focused ion beam scaning electron microscope

6 MV Van de Graaff-Pelletron ion accelerator TEM holder for tomography measurements Reverse action self closing fine tip tweezer

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March 23, 2020

Dear Dr. Phillip Steindel and JoVE editorial team,

We thank you and the five reviewers for the supportive review and suggestions to improve the quality of the manuscript. We have made our best effort to incorporate all the suggestions, combining several when overlap was identified. We believe this manuscript is strengthened as a result and as such thank you all for your time and insight. The following is our detailed response to each review:

Reviewer #1:

Manuscript Summary:

The manuscript provides a very comprehensive summary of the steps and protocol for conducting an in situ multi-beam TEM irradiation experiment. The paper covers basic topics in detail including selection of ion species, SRIM calculations, converting fluence/flux to dpa, etc. The manuscript also present different examples of irradiation experiments, how data may be collected and analyzed, and some representative results. Overall, the paper is a good summary of an emerging technique which can have broad implications in a number of fields.

Response:

The authors thank the reviewer for the kind view of the manuscript. We are especially appreciative of the views expressed on novelty and broadness of impact of the information presented.

Major Concerns:

Much of the content in Section 1 (and some in Section 2) is a re-summarization of information which is already well established in the field. While I do not notice anything incorrect in the summary, this reviewer was distracted by reading content which was not new. If possible, it might be more impactful to make this portion of the manuscript more brief, or at least more clearly differentiate the content which is unique and relevant specifically for in situ irradiation. I found the NEW content to be the most interesting and useful part of the manuscript.

Response:

We recognize that some of the background material covered in the early portions of the protocol are not novel. We have edited the introduction to be more brief by removing several sentences (lines 85-87, 89-91, 95-98) that cover content that is not new. The manuscript is intended to be able to guide a user that is less experienced with irradiation science through each step in the experiment. As such, we included a





- 2 -

solid background and foundation for those readers. We agree that the new information specific to in-situ irradiation experiments should be emphasized. Additions to the introduction on lines 141-145 have been made to address this.

Minor Concerns:

The authors have done a nice job emphasizing the importance of avoiding shadowing in two different places in the paper. This is likely very important and merits emphasizing. When using the FIB milling technique (Section 2.3), some scientists have been known to mount the TEM lamellae inside the V shaped posts on the grid (i.e. the two side posts in Fig. 3b). It could be worthwhile to add a specific statement in the manuscript which cautions an experimentalist from mounting the sample inside the V post, highlighting the likely risk of shadowing which would occur as a result.

Response:

The authors thank the reviewer for recognizing the importance of the placement of the FIB lamellae. We agree that some scientists prefer the V shaped mounting location and that this should be addressed more clearly. A sentence emphasizing the risk of mounting in the V configuration has been added into section 2.3.2, line 426.

Reviewer #2:

Manuscript Summary:

The manuscript entitled "Sample Preparation and Experimental Design for in situ Multi-beam Transmission Electron Microscopy Irradiation Experiments" presents the methodology and design of the coupling of ion irradiation and electron microscopy to study the processes surrounding radiation damage. The information provided will be very valuable to future users of the facility as well as those designing new facilities for the same scientific purpose. The manuscript is well written and articulate. Therefore, this reviewer recommends minor revisions of the paper in its current form.

Response:

The authors thank the reviewer for the positive view on the usefulness of the protocol for users. Additionally, we are excited by the comments on inspiring and guiding design of future facilities.

Major Concerns:

Calculation of displacement damage: The thin lamella surfaces act as a strong sink for point defects [1], suppressing the steady state concentration of defects compared to a bulk irradiation. How is this accounted for in the in situ experiment and the calculation of displacement damage?

Response:

We agree with the reviewer that the application of in-situ TEM irradiation is not to replace or reproduce exact irradiated microstructures from bulk scale ion irradiation or neutron irradiations. The utilization of in-situ TEM, as noted recently in [Ref. 1], becomes valuable alongside bulk irradiation for understanding dynamical effects (for example: dislocation loop growth, dislocation faulting/unfaulting reactions, phase transitions, and defect-grain boundary interactions). Additionally, although the free surface will affect the defect concentration and evolution, previous in-situ ion irradiation research at the IVEM-Tandem has shown that this can be quantified [Ref. 2] through careful through thickness defect quantification. We have added the following paragraph addressing these concerns in the introduction section, Lines 151-157:

"The utilization of in-situ TEM irradiation creates an ideal scenario to watch the dynamic evolution of defects created in radiation environments. While this technique provides insight in

to defect evolution including loop faulting/defaulting reactions and defect-grain boundary (GB) accommodation mechanisms, significant experimental limitations exist in comparing the defect quantification to bulk scale irradiations due to well-known thin film effects including loss of point defect and defect clusters to the surface ^{19,20}."

Minor Concerns:

The formula presented on line 198 works for negative ion sources where the negative ion produced is a single element. However, many ion sources (such as the SNICS described in Section 3.1) are more fluent by producing a mixed element compound such as an oxide or hydride which then breaks apart in terminal of the tandem accelerator. In which case, the energy of the positive ion after tandem acceleration and breakdown of the compound in the terminal is proportional to the masses of the two elements in the compound. If this occurs with the experimental setup described in the review, such as possibly with AgO sources, then the formula on line 198 should be revised.

Response: Thank you for highlighting this case. The I³TEM facility does make use of multi-elemental sources. Equation (1) on Line 234 has been revised to address the case of using mixed element compound sources.

Instead of using SRIM which is only on Windows to calculate displacement damage, could another software package such as the faster Monte Carlo program IRADINA [2,3] be used?

Response: IRADINA is a powerful and flexible simulation code. SRIM is described here due to its widespread use in the community making comparison to existing work more straightforward. Additionally, this procedure is aimed towards users with little or no experience, and the SRIM user interface is much more straightforward and easier to implement.

How would the use of scanning TEM (STEM) with a low dwell time impact the experiments described instead of using conventional TEM?

Response: STEM with a low dwell time would likely be able to achieve a lower overall electron dose compared to conventional TEM. This may be advantageous for materials that are sensitive to knock on events and other forms of radiation damage from high energy electrons as shown in this study on liquid low dose STEM [Ref. 3]. A note clarifying this advantage has been added to 4.1.5, lines 534-537.

Are there references for the environmental stages and the stages for specialized mechanical testing? They should be added to sections 1.4.3 and 1.4.4.

Response: References have been added to 1.4.3 and 1.4.4 to aid reader in finding further information for the different stages.

The use of electropolishing (Section 2.4) may also induce its own issues. Uneven thickness can occur from dissimilar polishing or etching rates between phases of a material. Large thickness gradients can happen in TEM area from jet-polishing 3mm discs. There is also the potential to destroy the previous microstructure if performed on a previously irradiated specimen, such as inducing cavity growth from localized pitting during the electropolishing. Electropolishing is still a preferred method, but not the best for several circumstances. The wording should be clarified.

Response: We agree that preparing TEM samples via electropolishing has its own set of benefits and limitations. Wording in section 2.4 has been changed to clarify the specific benefits and limitations of electropolishing.

A comment on section 3.1.2: Beam profile monitors are generally seen as qualitative measures of the ion beam flux as the electron output and collection from the ion beam striking the filament is not a direct linear correlation. Could more quantitative measures, such as measuring the ion beam flux in a Faraday cup prior to a suppressed aperture be used?

Response: Section 3.1.2 has been changed to more clearly communicate that the Faraday cup is the preferred method of beam current measurement. Additional clarification on the benefits and drawbacks of using the beam profile monitor has also been added on line 464.

Reviewer #3:

Manuscript Summary:

Very useful protocol on sample preparation for in situ TEM characterization and for designing experiments for in situ ion irradiation using the I³TEM facility and similar facilities around the world. Very useful examples are provided.

Response:

Thank you for the kind view on the protocol and positive outlook on its usefulness.

Major Concerns:

In Section 1.3.2, the authors should reconsider recommending that the "Quick Calculation of Damage" option should be used. Further, they should make clear that the "quick K-P" mode in SRIM is not valid for multi-elemental targets. While the authors are correct that there are competing arguments regarding the use of "quick K-P" and "Full Cascade" options, the "quick K-P" option is a 60-year old approximation that that was derived by Lindhard only for the case of monoatomic materials and has no validity for multi-elemental targets. The "quick K-P" option as implemented does not account for energy transfers between different atoms in a multi-elemental target, which means it has no real physical basis no physical meaning. Unless, the authors want to restrict their protocol to simple metallic systems, they should provide clear guidance to readers who want to study compound semiconductors, intermetallics, complex ceramics, etc., where the "quick K-P" option has no physical basis or validity.

Response:

The topic of the use of quick K-P vs full cascade is an ongoing and important issue under debate in the community. As recently as February 2020 at the TMS conference, there is still heated debate. We see quick K-P as a valid and rapid method for quickly approximating damage events. We have edited the description of section 1.3 as well as in 1.3.2 to emphasize that the protocol, as written serves as a quick method for approximating the damage sufficient for planning in-situ ion irradiation experiments where the focus is on dynamics rather than total dpa. We have provided references to alternate methods more appropriate for reporting dpa data in final publication. We have emphasized that the most important part of the procedure is to record parameters such that they can be replicated.

The descriptions (Sections 1.3.5, 1.3.7 and 1.3.8) should be revised. As written, they seem relevant only to metals and the use of the "quick K-P" option in SRIM. ASTM E521 is a good reference for some metals, but is not a good reference for many compounds and ceramics. The authors may want to provide

some guidance on how to obtain displacement energies for materials not in ASTM E521. In compounds, intermetallics and complex ceramics, replacement events can result in anti-site defects, and the determination of displacements should include the replacements (NOVAC.txt file). The author should consider rewording Section 1.3.7 to read "VACANCIES by RECOILS for each target atom at each depth" for "Full Cascade" calculations.

Response: We thank the reviewer for the extensive explanation on how to better clarify the SRIM modeling protocol. Descriptions have been added to 1.3.5 to provide more insight to the reader on how to find threshold displacement energies not found in ASTM E521. Section 1.3, 1.3.6, and 1.3.7 have been edited to provide greater clarity.

Minor Concerns:

Some minor copy-editing is needed. On line 245, suggest inserting "over" after "range" to read "range over".

Response: Thank you for catching this error. Line 245 has been edited to read more clearly.

Line 353, suggest inserting "are" after "FIB".

Response: Thank you for catching this error. Reworded section 2.3 to be clearer.

Under Section 2.4, line 357, suggest inserting "metallic" after bulk (while obvious, electro polishing is limited to metallic materials and should be made clear in this protocol).

Response: Wording in section 2.4 has been changed to clarify the specific benefits of electropolishing.

Reviewer #4:

Manuscript Summary:

The manuscript is focusing on the sample preparation and experimental design for in situ experiment in TEM. It appears to indicate the detail of experimental design and preparation, but it seems not to mention or insufficient on concrete sample preparation for in-situ observation experiment for irradiation damage study. Reviewer recommends to revise this manuscript. Reviewer's comments are indicated as below.

Response:

Thank you for the kind words regarding the experimental design and preparation included in the protocol. The reviewer's comments on the importance of preparation specifically for damage evolution are useful and are addressed below.

Major Concerns:

This manuscript may need to specifically indicate not only advantages but also disadvantages of in situ experiment should be mentioned, for instance, the surface effect of thin foil on the observed phenomena, such as excess surface and boundary diffusion, less defect cluster nucleation, and more or less mechanical property change compared to bulk samples, extra defects produced during sample preparation, etc. The author can suggest some technical preparation methods to solve or avoid those problems. For example, the preparation method to make a better sample for in-situ observation should be concretely mentioned, such as flush polishing, gentle mill etc. for removal of surface damage produced by FIB.

Response: We agree with the reviewer that specific advantages and disadvantages should be addressed and have made several changes throughout the paper to highlight this difference. However, we would like to emphasize that this is not intended to be an article on the pro and cons of in-situ TEM. Those arguments should be presented in in-situ TEM or ion irradiation reviews and have been previously reported. This article is on the actual design of experiment and protocol for performing an actual in-situ ion irradiation TEM experiment. The specific advantages and disadvantages have been addressed with the addition of a paragraph in the introduction that describes the ideal uses and limitations of in-situ irradiation TEM experiments with a specific focus on the defect quantification in comparison to bulk specimens, lines 150-157. Specific considerations in FIB sample final polishing to minimize damage have been added to 2.3.3.

Minor Concerns:

1) E, q, VT, Vs, etc. in text should be indicated in Italic.

Response: Thank you for catching this typographical oversight on our part. The appropriate changes have been made on lines: 232, 236, 237, 305.

2) Figure 4(a) seems not to be well drawn as the rotation angle of 30 degree as indicated (b).

Response: Figure 4(a) has been modified to more clearly represent an angle of 30 degrees.

3) Figure 7, there must be a better example of microstructure evolution under irradiation.

Response: There are several publications that depict microstructure evolution under single beam irradiation cited on line 501. This example was chosen as it complements one of the only examples of microstructure evolution from simultaneous multibeam irradiation seen in figure 8. We want to emphasize the unique capability of simultaneous multiple ion beam irradiation.

4) Figure 8, again, it does not seem an appropriate examples on cavity formation and growth behavior.

Response: There are several publications that depict microstructure evolution under single beam irradiation cited on line 578. This study was chosen as it is one of the only examples of microstructure evolution from simultaneous multibeam irradiation. Again, we want to emphasize this unique application.

5) 3.2 can be merged with 3.1.

Response: The authors recognize that many of the steps in 3.2 are the same as in 3.1. However, there are enough unique considerations in the Colutron accelerator procedure that a separate section is needed to communicate these important differences between the two systems.

Reviewer #5:

Manuscript Summary:

This is a well written true prescription for in-situ TEM execution and observation with simultaneous single and multiple ion beam irradiation. The authors provide easy to follow steps to accomplish this process, including multiple pictures and enough details t be easy to replicate and confirm the accuracy. Note: I am not a microscopist, and could not venture a critique of the specific TEM parts and TEM sample preparation.

Response: We thank the reviewer for his insight and useful scientific feedback despite not being a microsocpist. The perspective is great to have.

Major Concerns:

None

Minor Concerns:

Line 170: "Damage type is determined by the kinetic energy of the ions with higher energies producing larger damage" - MAYBE deeper region of damage?

Response: The damage produced by higher energy ions results in a larger damage region, which means wider as well as deeper.

Line 206: How do you address and monitor the heating of the specimen? perhaps is addressed later?

Response:

Clarification has been added for temperature control during in-situ experiments in 1.4.1.

Line 253: How do you cool/keep sample to RT?

Response: This is an important consideration. Sentence added to 1.4.1 to address this question.

Line 370: Maybe mention how you compensate the ion beam displacement by the magnetic field of the TEM?

Response: Clarification in 3.1.1 has been added to specify that TEM conditions during alignment should match those used during the experiment to minimize the effects of the TEM magnetic field on the ion beam.

Line 380: how do know the beam distribution when it hits the samples? Is it a Gaussian or uniform on the area it hits?

Response: The beam distribution is captured in the burn spot where the center is darker and fades to the outer edge. It is typically assumed to be Gaussian in distribution, but nuances can be seen in the individual burn spot variations.

Line 404: How do estimate the correct mixture ratio for the light ions and how do you measure the current from these light ions?

Response: For triple beam experiments, the relative concentration of light ions generated in the Colutron accelerator can be roughly controlled using the feed gas mixtures. The beam current from each accelerator can be independently measured to calculate the relative dose of each beam.

Line 406: I don't think that using 10 keV light ion beams would cause and cross-talk to the 10 MeV ions. The cross-talk is insignificant.

Response: We agree there is no significant cross talk between ions. However, in the I³TEM facility, activating the bending magnet that steers the ions from the Colutron accelerator to be co-linear with the

Tandem accelerator will affect the ions from the Tandem, and additional corrections will need to be made due to this change.

We thank all five reviewers and the JoVE editorial team for all of their comments and suggestions. We believe the manuscript is significantly stronger as a result and of greater impact to the community.

References used in the review:

- [1] C.J. Ulmer, A.T. Motta, Characterization of faulted dislocation loops and cavities in ion irradiated alloy 800H, J. Nucl. Mater. 498 (2018) 458-467. doi:10.1016/j.jnucmat.2017.11.012.
- [2] Li, M., Kirk, M., Baldo, P., Xu, D. & Wirth, B. Study of defect evolution by TEM with in situ ion irradiation and coordinated modeling. Philosophical Magazine 92, 2048-2078 (2012).
- [3] Abellan, P. et al. Factors influencing quantitative liquid (scanning) transmission electron microscopy. Chemical Communications 50, 4873-4880 (2014). DOI: 10.1039/C3CC48479C

Sincerely,

Khalid Hattar, Ph.D.

Center for Integrated Nanotechnologies

Sandia National Laboratories

Khalid Hattar



Operated for the U.S. Department of Energy's National Nuclear Security Administration by National Technology & Engineering Solutions of Sandia, LLC (NTESS)

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> > Formatted: Tab stops: 4.6", Left + Not at 4.88" + 5.25"

March 23, 2020

Dear JoVE Editor,

We thank you and the reviewer for the supportive suggestions to improve the quality of the manuscript. We have made our best effort to address or incorporate all the suggestions. We believe this manuscript is better prepared for visual presentation as a result and as such thank you all for your time and insight. The following is our detailed response to each reviewcomment:

Line 99, Deuterium has been defined with symbol D for clarity.

Line 133, page break has been removed.

Section 2.2.1, line 367 has been updated to provide more information on possible solvent selection.

Section 3.1.2, line 443 has been updated with more details to clarify the steps taken.

Section 3.1.2.1, line 447 has been updated with more details to clarify the steps taken.

Section 3.1.2.1, line 451 has been updated with more details to clarify the steps taken.

A reference to a later figure on Line 471 has been removed.

Section 4.1.3 line 525 has been updated with a more detailed description to clarify steps taken.

Section 4.1.4, line 532 has been updated with more detailed steps.

Section 4.1.5 line 537 has been updated with a suggested imaging condition. The steps to achieve each

individual imaging condition are covered at length in several books and publications and are considered to be well known procedures and outside the scope of this protocol.

Section 4.1.7, line 552, has been updated to clarify that each in situ holder has unique steps for operation, and their respective manuals should be consulted.

Line 563, the gun chamber vacuum threshold is different for all microscopes and can also depend on the type of filament or emission source. A line has been added that the user should consult the manufacture specifications.

Section 4.2.1, line 571, has been updated to the imperative voice.

Line 574, "precessed" is the correct word, stemming from "precession", the change in orientation of the rotational axis of a rotating body.

Line 636, MEMS has been defined as microelectromechanical system.



Exceptional Service in the National Interest

- 2 - March 23, 2020

Line 651, specific brand of picoindenter has been removed leaving only the general tool name. The materials table has been updated with several holders that have been used in the representative results.

Figure legends, lines 671-721, titles have been updated at the suggestion of the reviewer.

Sincerely,

Khalid Hattar, Ph.D. Center for Integrated Nanotechnologies Sandia National Laboratories

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