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A novel biaxial testing apparatus for the determination of forming limit under hot stamping conditions --Manuscript Draft--

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Abstract:	Hot stamping and cold die quenching is increasingly used to form complex shaped structural components of sheet metals ¹ . Conventional experimental approaches, such as the out-of-plane and the in-plane tests, are not applicable to the determination of forming limits when heating and rapid cooling processes prior to forming are introduced for testing under hot stamping conditions. A novel in-plane biaxial testing system was designed and used for the determination of forming limits of sheet metals at various strain paths, temperatures and strain rates after rapid heating and cooling processes in a thermo-mechanical materials resistance heating uniaxial testing machine, Gleeble. The core part of the biaxial testing system is a biaxial apparatus which is adopted to transfer the uniaxial force provided by the Gleeble uniaxial machine to a biaxial force. One type of cruciform specimens was designed and verified for the formability test of aluminium alloy 6082 by using the proposed biaxial testing system. Digital image correlation (DIC) system with a high-speed camera was adopted for strain measurement on a specimen during a deformation history. The aim of proposing This biaxial testing system is to enables forming limits of an alloy to be determined at different temperatures and strain rates under hot stamping conditions.
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Dear Editor,

Thank you so much for the editorial comments which are very valuable. The manuscript has been modified according to the comments, which have been detailed in the file of "Response to editorial comments". I would very much appreciate if you could consider the original work presented in the paper to be published in your journal. We look forward to hearing from you.

Sincerely,



Nan Li

TITLE:

A novel biaxial testing apparatus for the determination of forming limit under hot stamping conditions

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KEYWORDS:

Biaxial tensile test, biaxial apparatus, forming limit, formability, hot stamping, sheet metal forming

SHORT ABSTRACT:

This protocol proposes a novel biaxial testing system used on a resistance heating uniaxial tensile test machine in order to determine the forming limit diagram (FLD) of sheet metals under hot stamping conditions.

LONG ABSTRACT:

Hot stamping and cold die quenching are increasingly used to form complex shaped structural components out of sheet metals. Conventional experimental approaches, such as out-of-plane and in-plane tests, are not applicable to the determination of forming limits when heating and rapid cooling processes are introduced prior to forming for tests conducted under hot stamping conditions. A novel in-plane biaxial testing system was designed and used for the determination of the forming limits of sheet metals at various strain paths, temperatures, and strain rates

after rapid heating and cooling processes in a resistance heating uniaxial testing machine. The core part of the biaxial testing system is a biaxial apparatus, which transfers a uniaxial force provided by the uniaxial machine to a biaxial force. One type of cruciform specimen was designed and verified for the formability test of aluminum alloy 6082 using the proposed biaxial testing system. A digital image correlation (DIC) system with a high-speed camera was used for taking strain measurements of a specimen during a deformation. The aim of proposing this biaxial testing system is to enable the forming limits of an alloy to be determined at various temperatures and strain rates under hot stamping conditions.

INTRODUCTION:

The automotive industry is facing a huge global challenge of reducing fuel consumption and minimizing environmental pollution from vehicle emissions. Weight reduction is beneficial to improving the performance of automobiles and can directly reduce energy consumption¹. Due to the low formability of sheet metals at room temperature, hot stamping and cold die quenching processes (referred to as hot stamping)² are used to improve the formability alloys and thus to obtain complexly shaped components in automotive applications.

A forming limit diagram (FLD) is a useful tool to evaluate the formability of an alloy³. Out-of-plane tests, such as the Nakazima test^{4,5}, and in-plane tests, such as the Marciniak test⁶⁻⁸, are conventional experimental methods to obtain the FLDs of sheet metals under various conditions⁹⁻¹¹. A servo-hydraulic biaxial testing machine has also been used to investigate the formability of alloys at room temperature^{12,13}.

However, none of the methods above are applicable to formability tests under hot stamping conditions, since a cooling process prior to forming is required along with control of the heating and cooling rates. The deformation temperature and strain rate are difficult to obtain accurately. Therefore, a novel formability testing system is proposed in this study to experimentally determine the forming limits of sheet metals under hot stamping conditions.

PROTOCOL:

1. Preparation of specimens

1.1) Machine flat dog-bone and cruciform specimens from commercial material aluminum alloy 6082 (AA6082) using a laser cutter and a computer numerical control (CNC) milling machine (for formability tests at different strain paths including uniaxial, plane strain, and equi-biaxial straining states).

1.2) Measure the thickness of each cruciform specimen and each dog-bone specimen with a vernier caliper three times in the central gauge region and calculate the average values. Ensure that the thickness of the gauge section in a cruciform specimen is 0.7 ± 0.05 mm and that the thickness of the uniaxial specimen is 1.5 ± 0.1 mm.

1.3) Spray-paint the entire top surface of a cruciform specimen by using a flame-resistant, black

spray paint (capable of withstanding temperatures up to 1,093 °C). Wait until the paint dries and then spray flame-resistant, white paint dots from arm's length to create a stochastic spraying pattern to be recognized by the DIC system (see the example in Figure 1).

1.4) Weld a pair of thermocouples to the center of the back surface (opposite to the painted surface) of the specimen. Connect the other end of the thermocouple to the feedback temperature control system of the uniaxial testing machine to monitor and control the temperature change history.

2. Assembly of the biaxial testing apparatus

2.1) Assemble all parts of the biaxial testing apparatus, including a base plate, a central shaft, input and output rotatable plates, carriages, a clamp, guide rails, and rigid connecting rods (the assembled apparatus is shown in Figure 2).

2.1.1) Using a connecting rod, couple the input rotatable plate directly to the movable jaw of a resistance heating uniaxial tensile test machine, which provides the uniaxial tensile force. Couple the machine to the central drive shaft and couple this central drive shaft to the output rotatable plate.

2.1.2) Ensure that the rotation of the input rotatable plate around the axis of rotation rotates the drive shaft, thereby rotating the output rotatable plate to which it is coupled around the axis of rotation.

2.1.3) At one end, couple each of the rigid connecting rods to one of the connection points on the output rotatable plate. Couple the other end to one of the carriages.

Note: This will cause the carriages with specimen holders to slide back and forth along the guide rails with low friction, which can apply a biaxial force to the cruciform specimen.

2.1.4) Using screw bolts, clamp each arm of the cruciform specimen to a carriage with a specimen holder and a top plate.

2.2) Set up grips in the chamber of the uniaxial tensile test machine, as shown in Figure 3 (a). Attach four welding cables to each pair of grips, which are made of stainless steel and copper, respectively, and thus connect the welding cables to the electrical power supply.

Note: The conductor area of the welding cables is 50 mm² and the current rating is 345 A.

2.2.1) Put the grips and the clamp of the biaxial testing apparatus into the two jaws of the uniaxial tensile test machine and tighten them inside (Figure 3 (a)).

2.3) Set up the biaxial testing apparatus in the chamber of the uniaxial tensile test machine, as shown in Figure 3 (b).

2.3.1) Use two frames and screw bolts on the top and the bottom sides of the base plate to fix the apparatus in the chamber of the uniaxial tensile test machine.

2.3.2) Put the specimen into the specimen holder on top of the biaxial testing apparatus.

2.3.3) Connect each terminal of the welding cables to each clamping region of the specimen.

3. Setup of the heating and quenching system

3.1) Tightly connect each clamping region of the specimen to the stainless steel top plate, which serves as the electrode for resistance heating.

3.2) Tighten the welding cables with crimp ring terminals to the top plate of each clamping region.

3.3) Connect flared nozzles with hoses to the high flow quench system with regulated air supply at 8,000 kg/m² pressure for cooling.

3.4) Use four nozzles to blow air from the arms of the specimen to the central region of the specimen.

Note: The nozzles are not directed onto the gauge section for cooling to avoid blocking the central zone from the camera's view.

4. Setup of the DIC system

4.1) Connect the high-speed camera of the DIC system with a micro lens to a computer. Adjust the frame rates of the camera to 25 fps, 50 fps, and 500 fps from the menu of frame rates (for the tests at the stretching strain rates of 0.01/s, 0.1/s and 1/s, respectively). Set the resolutions of all images to 1,280×1,024 pixels.

Note: The frame rates depend on the number of data points to be collected; at least 200 data points can be collected using the above settings.

4.2) Use an additional spotlight with a power of 300 W for tests at high strain rates. Point the spotlight directly at the chamber of the uniaxial tensile test machine.

4.3) Adjust the camera lens so that it is parallel to the top surface of the specimen in the chamber and focus the camera on the gauge section.

5. Experimental program

5.1) Run the resistance heating uniaxial tensile test machine by clicking the triangular run

button in the control software.

Note: Electricity runs through the AA6082 material and heats it to the solution heat treatment temperature of 535 °C¹⁴ at a heating rate of 30 °C/s. The material is soaked at 535 °C for 1 min, which is sufficient for the full resolution of precipitates. Air blowing from the quench system is used to quench the material at a cooling rate of 100 °C/s¹⁵ to one of 3 designated elevated temperatures in the range of 370-510 °C.

5.2) Stretch the specimen with the biaxial testing apparatus at a constant strain rate in the range of 0.01-1/s and record the deformation history by manually pressing the trigger button connected to the high-speed camera.

Note: The input displacement from the uniaxial testing machine to the biaxial testing apparatus was controlled by the built-in software of the uniaxial testing machine.

5.3) Perform the tests at different strain paths consisting of uniaxial, plane strain, and biaxial states³ by adjusting the configuration of the biaxial testing apparatus.

5.3.1) Disconnect two opposed connecting rods for uniaxial tests. Clamp a dog-bone specimen on the biaxial testing apparatus and connect it to welding cables, as in steps 3.1-3.4. Repeat steps 5.1-5.2.

5.3.2) Fix two opposed carriages to the base plate with screw bolts to restrict the deformation on the corresponding direction for testing under plane strain state. Clamp a cruciform specimen on the biaxial testing apparatus and connect it to welding cables, as in steps 3.1-3.4. Repeat steps 5.1-5.2.

5.4) Repeat steps 5.3.1-5.3.2 for each test condition three times, using new dog-bone and cruciform specimens.

6. Data processing

6.1) Import all images recorded by the high-speed camera into the post-processing software and follow standard steps for data analysis according to the software manual.

6.2) Use the ISO standard³ to determine the forming limits by clicking the FLC Mode button in the software.

Note: This method has already been integrated into the image correlation processing software.

6.3) Mark each result of the forming limits at various temperatures, strain rates, and strain paths in a diagram.

6.4) Plot the forming limit curves at all test conditions to obtain an FLD of an alloy under hot

stamping conditions.

REPRESENTATIVE RESULTS:

Since FLDs are highly strain path-dependent, the linearity of the strain path for each test condition was verified by analyzing the DIC results; the strain paths are proportional throughout deformation for each test condition. The range of the minor-to-major strain ratio is approximately -0.37 (uniaxial condition) to 0.26 (near equi-biaxial condition). By processing data for different AA6082 conditions, forming limit data for different strain paths were determined and hence, the FLDs for AA6082 at hot stamping conditions were obtained through curve fitting. In Figure 3, forming limit data were obtained at various temperatures, strain rates, and strain paths after the heating and cooling processes. The fitted dashed lines indicate the formability of this alloy, AA6082. A forming limit curve identifies the boundary between uniform deformation and the onset of plastic instability or diffuse necking, which lead to failure. The region above the curve represents potential failure, and the region below the curve is regarded as a safety region, where uniform deformation occurs at the corresponding testing conditions. A higher FLC indicates that the material has better formability if the shape remains the same.

Formability tests using the novel in-plane biaxial tensile testing system were conducted at the designated deformation temperatures and strain rates after the heating and cooling processes. It was found that, when the strain rate increases from the designated strain rate of 0.01/s to 1/s, the forming limit of AA6082 increases. The forming limit has a larger increase, from 0.1/s to 1/s, than from 0.01/s to 1/s, as shown in Figure 4 **Error! Reference source not found.**(a).

In Figure 4 (b), there is a monotonic increase in the forming limit from 370 °C to 510 °C. This indicates that high formability of AA6082 can be obtained at a higher temperature under hot stamping conditions. The three forming limit curves are quite close to each other on the left side of the FLD, which means that the sensitivity of temperature dependence is larger for tension-tension biaxial strain paths than for tension-compression strain paths.

Figure 1: An example of a stochastic pattern in a cruciform specimen before biaxial stretching (a) and after biaxial stretching (b). The pattern with white dots on a black background is captured by the high-speed camera during tests. The size and density of the speckles within a pattern are subjected to the standard requirements of DIC analysis¹⁵.

Figure 2: The assembled biaxial testing apparatus. The apparatus includes a base plate, a central shaft, rotatable plates, carriages, guide rails, and connecting rods. It is mounted in the chamber of the resistance heating uniaxial testing machine. Key components have been marked on the figure.

Figure 3: Setup of grips and the biaxial testing apparatus in the chamber of the uniaxial testing machine. (a) The grips and the clamp. (b) The biaxial testing apparatus and nozzles for air cooling.

Figure 4: FLDs of AA6082 at different strain rates and different temperatures under hot stamping conditions. The symbols are the results of the forming limits under different conditions. The dashed lines were obtained through the polynomial fitting algorithm.

DISCUSSION:

Conventional formability test methods used to determine forming limits are usually applicable only at room temperature. The presented technique can be used to evaluate the formability of metals for hot sheet stamping applications by introducing a novel biaxial testing apparatus to a resistance heating uniaxial testing machine. This cannot be performed using conventional methods for hot stamping applications. The setup of heating and cooling systems and the DIC system is critical to controlling the uniformity of temperature distribution in a specimen and thus to recording the deformation history of stretching specimens.

In this technique, the heating and cooling rates can be precisely controlled by a resistance heating method for complex forming process applications. The biaxial mechanism has a relatively simple configuration, which reduces the cost and complexity of biaxial tensile testing compared to traditional biaxial testing mechanisms. However, temperature fields made by resistance heating are affected by specimen design in this testing system, and temperature gradients on a specimen cannot be avoided. No existing standard specimen design is available for biaxial testing.

In summary, this is the first time an FLD of alloys under hot stamping conditions was obtained. High forming speeds and high temperatures within the designated ranges are beneficial for enhancing the forming limits of AA6082 under hot stamping conditions. This novel technique can be used to determine the forming limits of metal sheets under complex testing conditions. The obtained experimental results can be used to develop a material model that predicts the thermo-mechanical behavior and the formability of an alloy. The mechanism of the apparatus can be modified to conduct formability tests subjected to non-linear strain paths in the future.

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DISCLOSURES:

The authors have nothing to disclose.

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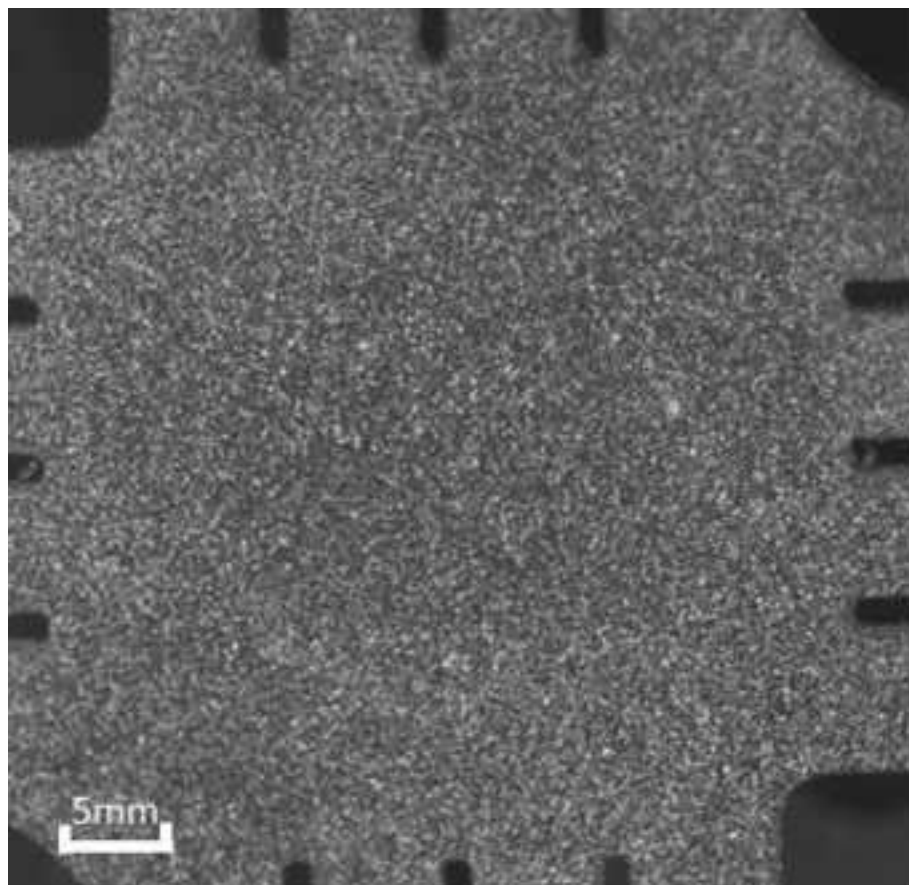
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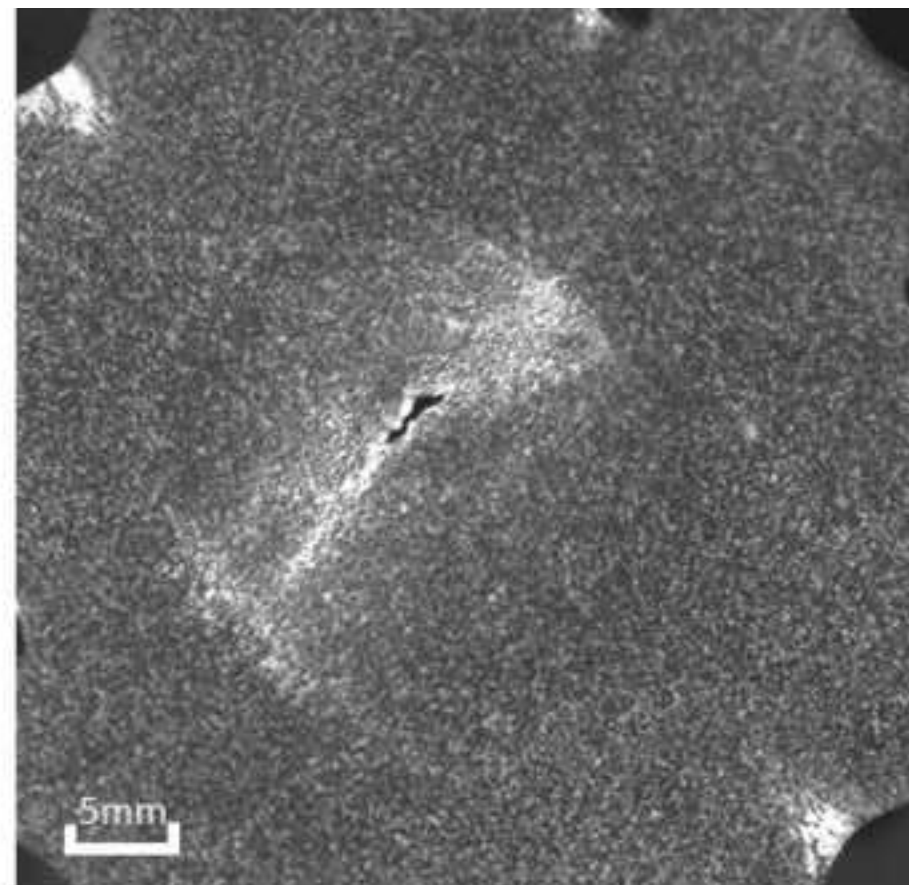
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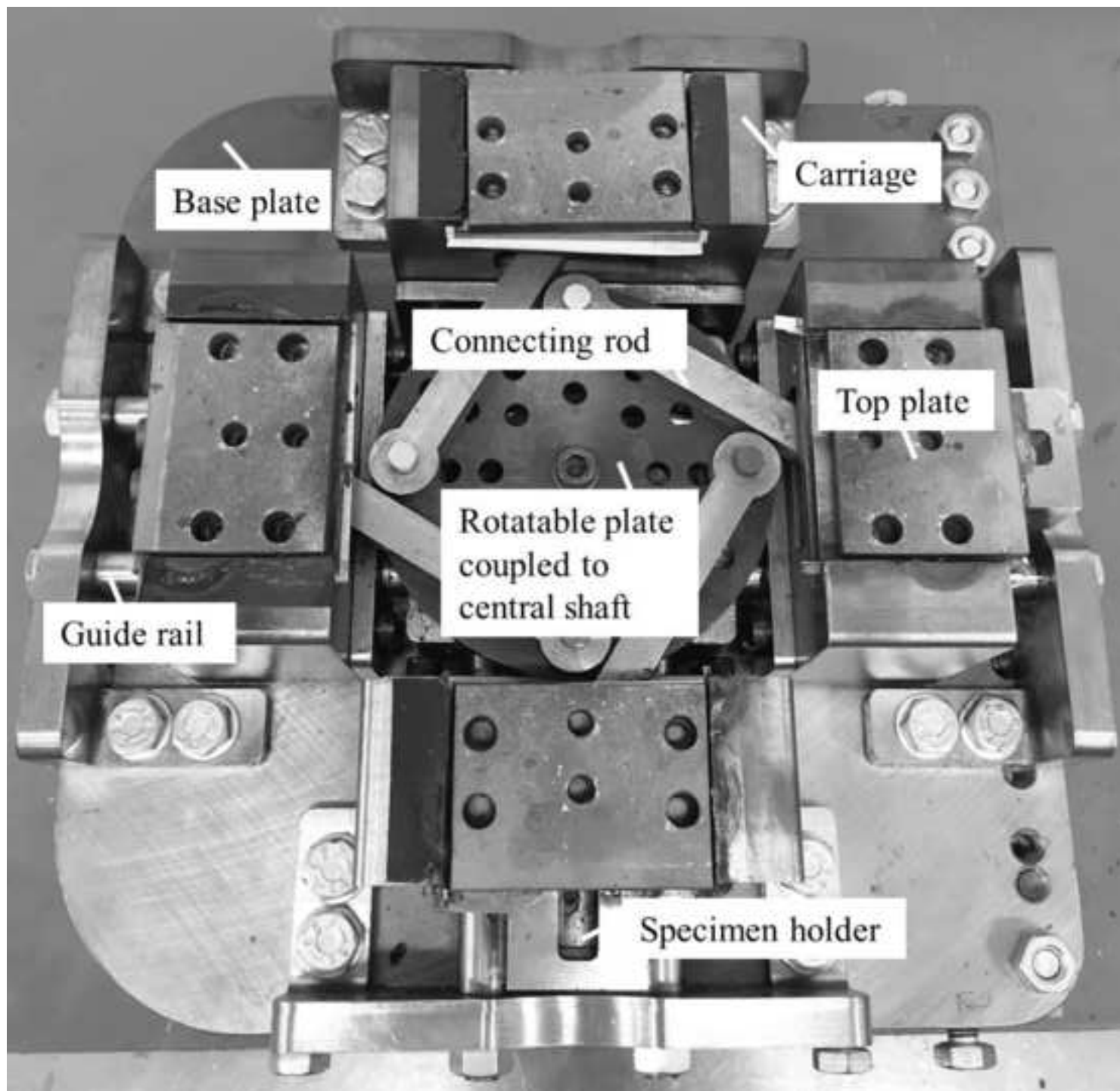
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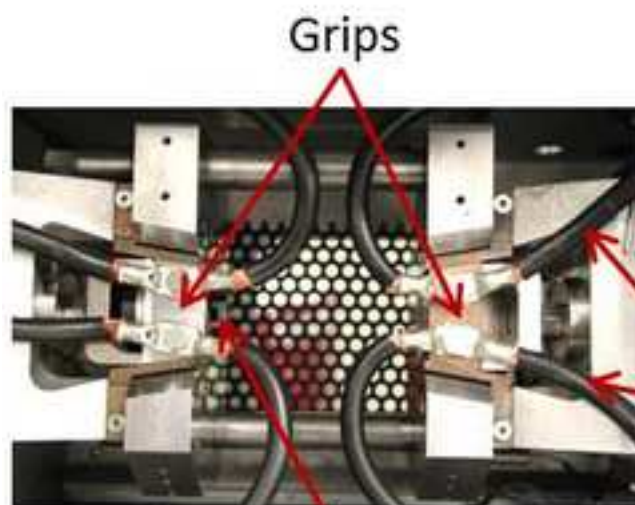


(a)



(b)



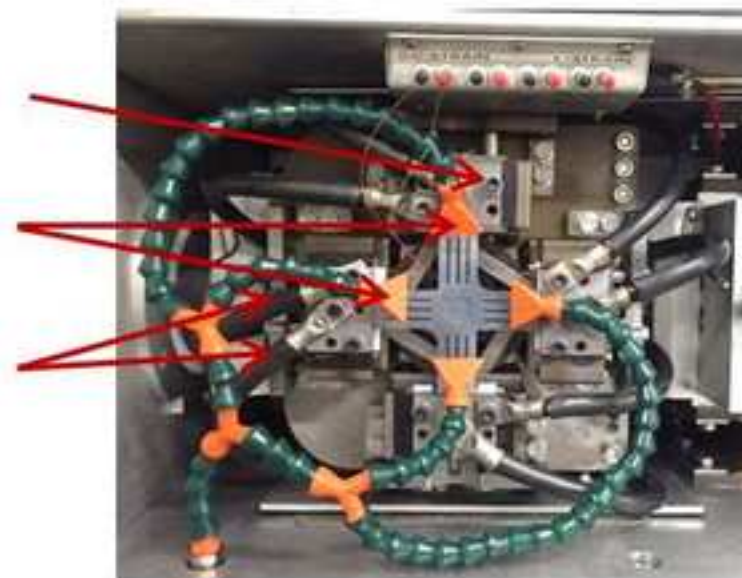


Grips

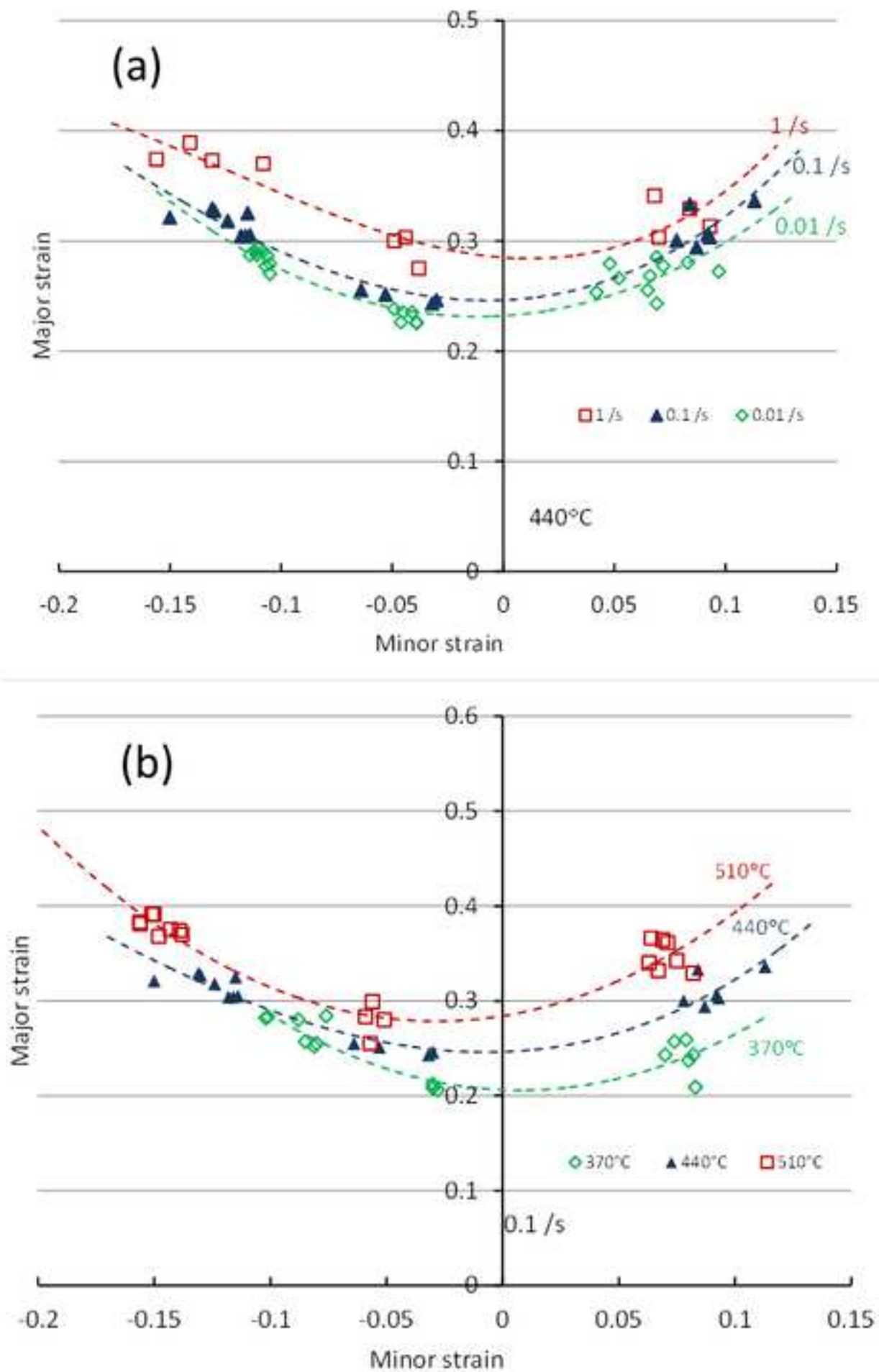
Clamp

(a)

Top plate
Flared nozzles
Welding cables



(b)



Name of Material/ Equipment	Company	Catalog Number
Aluminium Alloy	Smiths Metal	6082
Laser cutter	LVD Ltd	HELIUS 25/13
CNC machine	HAAS Automation	TM-2CE
Vernier caliper	Mitutoyo	575-481
Resistance heating uniaxial testing machine	Dynamic System Inc	Gleeble 3800
High flow quench system	Dynamic System Inc	38510
Thermocouples	Dynamic System Inc	K type
Nozzles	Indexa	
Welding cables	LAPP Group	H01N2-D
High-speed camera	Photron	UX50
Camera lens	Nikon	Micro 200mm
Lamp	Liliput	150ce
Laptop	HP	Campaq 2530p
	Manufactured independently	
Biaxial testing apparatus		
Steel	West Yorkshire Steel	H13
Image correlation processing software	GOM	ARAMIS

Comments/Description

Specimens machining

Laser cutting specimens

Machine specimens by milling

Thickness measurement

Thermo-mechanical materials simulator

For air cooling

Nozzle flared 1/4 inch bore

For DIC testing

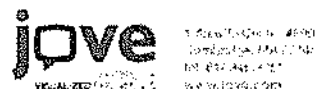
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For images recording

All parts were designed and machined by authors for biaxial testing

Materials of the biaxial testing apparatus

Non-contact measuring system and data post-processing



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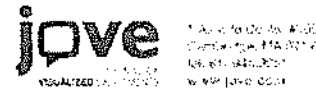
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 Signature: Nan Li Date: 25/09/2016

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Response to Reviewers' Comments

Editorial comments:

Changes to be made by the Author(s):

Protocol Step 5.2: How is the stretching done? Is this software controlled? Please mention the steps involved. This is essential to ensure that our scripting team can plan filming accordingly after the manuscript is accepted.

Thanks. This information has been added on P4.

Please ensure that your discussion covers the following in detail: 1) modifications and troubleshooting, 2) limitations of the technique, 3) significance with respect to existing methods, 4) future applications and 5) critical steps within the protocol.

Thanks. All has been covered. Information on 1) and 5) has been shown in the first paragraph of the Discussion section, p6. Information on 2) and 3) has been shown in the second paragraph. Information on 4) has been shown in the last paragraph.

After you have made all of the recommended changes to your protocol (listed above), please adjust the highlighting to identify 2.75 pages or less of text (which includes headings and spaces) that should be visualized to tell the most cohesive story of your protocol steps. Please see JoVEs instructions for authors for more clarification. Remember that the non-highlighted protocol steps will remain in the manuscript and therefore will still be available to the reader. Please bear in mind that the complete video filming process (if the manuscript is accepted) will be completed within one day (typically 6-8 hours).

Thanks. Text has been highlighted.

Grammar:

- Please copyedit the manuscript for article usage (a, an, the).
- Long abstract – “to enable determination of forming limits of an alloy various temperatures and strain rates”
- 5.2 – “the trigger button connected the high-speed camera”

Thanks. Grammar problems above have been corrected.

Visualization: 2.1 is confusingly labeled. Objects are plural even when a single object is indicated. Are there 4 of each specimen holder, carriage, and top plate? This is not clear and very confusing. Please also provide a photograph of the setup for step 2.2.1 and 2.3; this can be included as a supplemental file.

All have been changed to be singular noun. There are 4 carriages, specimen holders and top plates. They are identical in the figure. Figure 3 has been added.

Additional detail is required:

-1.1 – How is this done? Please provide a citation.

Laser cutting and milling are basic mechanical method to machine samples. Nothing is special here but just follow the standard steps of using the machines. Names of the machine are listed in the Materials table.

-1.2 – What is meant by “in gauge sections?”

Improved on p2. Gauge section is widely used to define the concerned region on a specimen.

-1.3 – What is used to spray the white dots? Is there a particular distance from the sample?

Information has been added on p2. The same spray as the black one, the name of spray had been listed in the Materials table.

-2.1.1 – How is coupling performed?

Information has been added on p3.

-2.1.4 – How is each arm clamped?

Each arm is clamped by screw bolts. This has been stated.

-2.2 – How does one set up grips?

Figure 3 has been added.

-2.3.2 – Which apparatus? Is the specimen put in the specimen holder?

Yes. This has been added.

-3.4 – What central region? It sounds as though air from the arms is being blown to the center of something. Is this what you mean?

Yes. This has been clarified.

Results:

-Figure 1 – Please include a scale bar.

Added as suggested.

-Figure 3 – Please define the symbols in the figure legend. It is not entirely clear which label goes with which condition in the chart.

Added as suggested.

Reviewers' comments:

Reviewer #1:

Manuscript Summary:

Good

Major Concerns:

No

Minor Concerns:

Could all the figures be with coloured images/artwork ?

Figure 1, the lens is only for black-white images recording. Figure 2, no colour of all metal components anyhow. Figure 3 and Figure 4 are in colour now.Thanks.

Additional Comments to Authors:

N/A

Reviewer #2:

Manuscript Summary:

This paper proposed a new experiment method for the determination of forming limit of sheet metals under hot stamping condition. The FLD obtained is important and useful for hot stamping at high speed and high temperature.

Major Concerns:

N/A

Minor Concerns:

In the last sentence of long abstract, it seems that at is missed before various.

This has been corrected.

Additional Comments to Authors:

several related papers maybe added in the references;

[1] Xiao-bo Fan, Zhu-bin He, Wen-xuan Zhou, Shi-jian Yuan, Formability and strengthening mechanism of solution treated Al-Mg-Si alloy sheet under hot stamping condition, Journal of Materials Processing Technology , 2016, 228: 179-185

[2] Xiaobo Fan, Zhubin He, Peng Lin, Shijian Yuan, Microstructure, texture and hardness evolutions of Al-Cu-Li alloy sheet during hot gas forming with integrated heat treatment, Materials & Design, 2016,94:449-456

[3] Xiaobo Fan, Zhubin He, Kailun Zheng, Shijian Yuan, Strengthening behavior of Al-Cu-Mg alloy sheet in hot forming-quenching integrated process with cold-hot dies, Materials & Design, 2015, 557-565

Ref [11] has been referred.

Reviewer #3:

Manuscript Summary:

Presented in this paper study provide insight into hot stamping problems. The presented technique can be used to evaluate formability of metals by introducing a novel biaxial testing apparatus onto a resistance heating uniaxial testing machine. The problem is of special significance to gain better insight into to determine forming

limits of metal sheets under complex testing conditions. Hence, it is an interesting problem from the point of view of metal forming.

Major Concerns:

N/A

Minor Concerns:

It is possible to make a number of criticisms. For example, Fig.2 showing the setup of the testing equipment is unclear. Improving the visibility of the principle of operation would be very helpful. Also the message resulting from Fig. 1 is insignificant. This is just some info about the DIC methodology. It would be better to present photos of the samples after the tests.

Figure 2 is just the assembly of the biaxial apparatus instead of the entire testing set-up. Figure 1 was added according to previous editorial suggestions and now a photograph after stretching has been added. Figure 3 is added to show the set-up clearly. Thanks.

Additional Comments to Authors:

N/A